



A 32-year Perspective on the Origin of Wind Energy in a warming Climate

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Accessibility

1	A 32-year Perspective on the Origin of Wind Energy in a warming Climate
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Abstract

Based on assimilated meteorological data for the period January 1979 to December 2010, the origin of wind energy is investigated from both mechanical and thermodynamic perspectives, with special focus on the spatial distribution of sources, historical long term variations and the efficiency for kinetic energy production. The dry air component of the atmosphere acts as a thermal engine, absorbing heat at higher temperatures, approximately 256 K, releasing heat at lower temperatures, approximately 252 K. The process is responsible for production of wind kinetic energy at a rate of $2.46 \, W/m^2$ sustaining thus the circulation of the atmosphere against frictional dissipation. The results indicate an upward trend in kinetic energy production over the past 32 years, indicating that wind energy resources may be varying in the current warming climate. This analysis provides an analytical framework that can be adopted for future studies addressing the ultimate wind energy potential and the possible perturbations to the atmospheric circulation that could arise as a result of significant exploitation of wind energy.

Keywords: origin of wind energy; warming climate; thermal engine; interannual variability

1. Introduction

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Global installed wind capacity reached an unprecedented level of more than 318 GW at the end 44 45 of 2013, of which approximately 35 GW were added in 2013, the highest level recorded to date. Wind power contributes close to 4 % to current total global electricity demand. In total, 103 46 countries are using wind power on a commercial basis. Based on current growth rates, the World 47 Wind Energy Association estimates that global wind capacity could increase to as much as 48 700 *GW* by 2020 [1]. 49 A number of studies have sought to assess the ultimate potential for wind-generated electricity 50 assuming that the deployment of turbines should not influence the potential source [2-8]. Using 51 52 data from surface meteorological stations, Archer and Jacobson [4] concluded that 20 % of the global total wind power potential could account annually for as much as 123 PWh of electricity, 53 equivalent to 7 times total current global consumption. They restricted their attention to power 54 that could be generated using a network of 1.5 MW turbines tapping wind resources from 55 regions with annually averaged wind speeds in excess of 6.9 m/s at an elevation of 80 m. Using 56 assimilated meteorological data, Lu et al. [5] argued that a network of land-based 2.5 MW 57 turbines restricted to non-forested, ice-free, non-urban areas operating at as little as 20 % of their 58 rated capacity could supply more than 40 times current worldwide demand for electricity, more 59 than 5 times total global use of energy in all forms. 60 61 Numerous groups have argued that large scale deployment of wind farms could potentially influence the circulation of the atmosphere, altering consequently the global wind energy 62 63 resources [9-16]. For example, Adams and Keith [16] tried to quantify the limitation of wind 64 energy extraction using a mesoscale model and compared their results with other studies using

global atmospheric models. The energetics of the entire atmosphere is different from the energetics of the mesoscale region considered by Adams and Keith [16]. It is essential to understand how kinetic energy of wind is created in the entire atmosphere.

Wind energy is essentially the kinetic energy held by the center-of-mass movement of a volume element of air. The movement of the air is driven primarily by the spatial gradient in heat input. Diabatic heating occurs mainly in the warm tropics, with diabatic cooling dominating at relatively cold mid and high latitudes. In this sense, following Carnot, the dry air component of the atmosphere acts as a thermal engine, converting heat to kinetic energy to sustain the general circulation against the force of friction. The standard approach to investigate the energetics of the atmosphere was introduced by Lorenz in 1955 [17]. A number of groups have analyzed the energetics of the atmosphere based on the Lorenz Energy Cycle [18-22]. However, the geographic distribution of kinetic energy production and the temporal variability have not as yet been quantified.

This study investigates the origin of wind energy, with a specific focus on the spatial distribution of sources, historical long term variations and the efficiency for kinetic energy production. From a mechanical perspective, kinetic energy can be produced or destroyed only by real forces [23]. In the case of an air parcel in the atmosphere, the real forces are: gravity, the pressure gradient force, and friction. From a thermodynamic perspective, the creation of wind energy in the atmosphere involves absorption of heat at high temperature and release at low temperature, following the operational principle of a thermal engine. The paper also analyzes the thermodynamic processes within the atmosphere, quantifying the key thermodynamic variables including the net rate of heat absorption and the efficiency for kinetic energy production. The analysis provides a historical perspective on the production of kinetic energy in the atmosphere

and an analytical framework for future studies exploring the ultimate potential for wind energy and potential for significant change in the circulation of the atmosphere as a consequence of future large scale turbine deployment.

2. MATERIALS

The study is based on meteorological data from the MERRA compilation covering the period January 1979 to December 2010. Kinetic energy of wind, wind speeds, air temperatures, geopotential heights and surface roughness were obtained on the basis of retrospective analysis of global meteorological data using Version 5.2.0 of the GEOS-5 DAS. We use the standard 3-hourly outputs of the free atmosphere conditions and the standard hourly outputs of the boundary layer conditions [24]. The multivariate ENSO index is from the National Oceanic and Atmospheric Administration (available at: http://www.esrl.noaa.gov/psd/enso/mei/).

3. Atmospheric kinetic energy

The kinetic energy corresponding to unit mass of the atmosphere is given by $|\vec{v}|^2/2$ where \vec{v} is the wind speed. The total and hemispheric atmospheric kinetic energy stocks may be obtained by integrating over the appropriate spatial domains. Composite results for monthly mean values and for the long-term variation of global kinetic energy are shown in Fig. 1. The inter-annual variation of the total kinetic energy stock is associated with the changing phases of the El Niño - Southern Oscillation (ENSO) cycle (Fig. 1a and Fig. 2). During the warm El Nino phase (notably years 1983, 1987, 1997 and 2010), elevated sea surface temperatures (SSTs) result in an increase in the kinetic energy stock; during the cold phase La Nina phase (notably years 1985, 1989, 1999 and 2008), colder SSTs contribute to a decrease. The global kinetic energy stock averaged approximately 1.50 MJ/m^2 over the past 32 years, 1.31 MJ/m^2 in the Northern Hemisphere with 1.70 MJ/m^2 in the Southern Hemisphere.

The spatial distributions of the annual mean, June - August, and December - February kinetic energy budgets are shown in Fig. 3. Clearly evident is the influence of the dominant storm tracks at midlatitude, and the steady components of the subtropical and polar jet streams. There are two distinct peaks in the Northern Hemispheric kinetic energy stock east of Japan and east of the North American continent, with a more continuous belt of high kinetic energy located between 30 °S and 60 °S in the Southern Hemisphere. As discussed by Huang et al. [25], the boundary layer wind, for example the wind at 100 m, is controlled by conditions in the free atmosphere, perturbed by fast varying turbulence in the boundary layer. Strong winds in the free atmosphere generally lead to strong winds near the surface, and consequently to high instantaneous values of the capacity factors for wind turbines. The spatial distributions in Fig. 3 reflect the geographic distribution and seasonality of wind resources as reported in the earlier studies [5, 26, 27].

4. Production of kinetic energy

For an air parcel of unit mass, production of kinetic energy may be written as:

$$\frac{dK}{dt} = -gw - \frac{1}{\rho}\vec{v}\cdot\nabla p + \vec{v}\cdot\vec{F} \tag{1}$$

where K is the kinetic energy corresponding to unit mass, g is the gravitational acceleration, w is the vertical velocity, \vec{v} is the velocity, ρ is the air density, p is the pressure and \vec{F} is the frictional force.

In calculating the kinetic energy production rate, it is convenient to consider the rate for production of kinetic energy in a fixed unit of volume. Re-organizing equation (1), we have:

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$$\frac{\partial \rho K}{\partial t} = -\nabla \cdot (K \rho \vec{v}) - \vec{v} \cdot \nabla p + \rho \vec{v} \cdot \vec{F} - g \rho w \tag{2}$$

The left hand side of this equation denotes the rate per unit volume for production of kinetic

energy. The right hand side defines contributions to the production rate associated with the convergence of the kinetic energy flux $(-\nabla \cdot (K\rho\vec{v}))$, and the work carried out or consumed by the pressure gradient force $(-\vec{v} \cdot \nabla p)$, friction $(\rho\vec{v} \cdot \vec{F})$ and gravity $(-g\rho w)$.

The atmosphere is in quasi-hydrostatic balance: gravity is balanced approximately by the vertical pressure gradient force. In this case, equation (2) may be recast in the simpler form:

$$\frac{\partial \rho K}{\partial t} = -\nabla \cdot (K \rho \vec{v}) - \overrightarrow{v_h} \cdot \nabla_h p + \rho \vec{v} \cdot \vec{F}$$
 (3)

- where $\overrightarrow{v_h}$ is the horizontal component of \overrightarrow{v} , and $\nabla_h p$ is the horizontal gradient of the pressure force. Production of kinetic energy in the atmosphere, C, can be estimated as $C = -v_h \cdot \nabla_h p$ [17-140 22].
 - Fig. 4 illustrates the distribution of kinetic energy production, C, averaged over the past 32 years in units of 10^{-3} W/kg. The tropical and subtropical region from 30 °S to 30 °N, dominated by the thermally direct Hadley circulation, is responsible for a net source of kinetic energy as indicated in Fig. 4a. The most prominent sources are located in the mid-latitude oceanic regions below the 800 hPa pressure level, notably in the Southern Hemisphere, as depicted in Fig. 4c. Production of kinetic energy in these regions is associated with the intense development of eddies that stir the atmosphere over the ocean, carrying cold air equatorward and warm air poleward, resulting consequently in cross-isobaric flow. The topographic forcing of the Tibetan plateau has a noticeable impact on the production of kinetic energy in the upper region of the atmosphere, from 0 $hPa \sim 600 \ hPa$, as indicated in Fig. 4b.

The global and hemispheric rates for production of kinetic energy are obtained by integrating the production term, C, over the entire atmosphere or over each hemisphere separately. The global kinetic energy production rate averaged over the past 3 decades is estimated at $2.46 \, W/m^2$, with

a upward trend since the late 1990s (Fig. 5a). The average rate for production in the Northern Hemisphere is $2.44 \, W/m^2$, $2.49 \, W/m^2$ for the Southern Hemisphere. Hemispheric production rates indicate strong seasonality (Fig. 5c), reaching maximum power output during local winter, with minima in local summer.

5. Dissipation

Motions of the atmosphere against friction convert kinetic to internal energy. This process is thermally irreversible, resulting in an increase in entropy. Approximately half of the frictional dissipation takes place within the lowest kilometer of the atmosphere, a result of turbulent motions generated mechanically by the flow over the underlying surface. The other half takes place higher in the atmosphere where small-scale disturbances are generated as a result of convection or shear instability of the vertical wind [28]. In the long run, the total kinetic energy in the atmosphere, KE, is determined by a balance between production, C, and dissipation by friction, D. The dissipation term may be quantified according to:

$$D = C - \frac{dKE}{dt} \tag{4}$$

The long-term variation and seasonal cycle of D are plotted in Fig. 6. Maximum dissipation occurs in February, corresponding to the peak in Northern Hemisphere kinetic energy reflecting the importance of surface roughness associated with Northern Hemisphere continental areas in dissipating kinetic energy. The entropy generation associated with dissipation can be approximated as $\frac{c}{T_{surface}}$, where $T_{surface}$ is the global average surface atmosphere (about 280 K). The fate of kinetic energy in the atmosphere from a mechanical perspective is summarized in Fig. 7. The residence time of kinetic energy, τ , calculated as KE/D, is 6.9 days.

6. The thermodynamics of atmospheric motions

According to the first law of thermodynamics:

$$C_p \left[\frac{\partial}{\partial t} T + \vec{v} \cdot \nabla T + \omega \left(\frac{\partial T}{\partial p} - \kappa \frac{T}{p} \right) \right] = Q \tag{5}$$

where Q defines the rate per unit mass of dry air for diabatic heating, C_P is the specific heat of the air, T is temperature, ω is the vertical component of wind velocity in an isobaric system and $\kappa = 0.286$ [29].

The annual mean spatial distribution of diabatic heating Q based on equation (5) is displayed in Fig. 8. The results presented here are consistent with earlier studies [30, 31]. An important fraction of the incoming sunlight reaches the surface which is heated accordingly. This heat finds its way back into the atmosphere as a result of turbulent transport through the atmospheric boundary layer. Most of the solar energy absorbed by the ocean is used to evaporate water. Water vapor in the atmosphere acts as a reservoir for storage of heat that can be released later. As the air ascends, it cools. When it becomes saturated, water vapor condenses with consequent release of latent heat. Heating is dominated in the tropical atmosphere by release of latent heat. Separate bands of relatively deep heating are observed at mid-latitudes where active weather systems result in enhanced precipitation and release of latent heat.

The atmospheric system consists of dry air and water. Its total entropy S^{total} and total static energy E^{total} , according to thermodynamics, can be expressed as: $S^{total} = S^{dry} + S^{H_2O}$ and $E^{total} = E^{dry} + E^{H_2O}$, where S^{dry} and E^{dry} represent the associated entropy and static energy of the dry air component and S^{H_2O} and E^{H_2O} represent the associated entropy and static energy of the water component. The focus in this study is on how atmospheric motion of the dry air is maintained by diabatic heating. Condensation and evaporation of water are treated accordingly as external to the dry air component [32], namely as an exchange of entropy and energy with the

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Regions of diabatic cooling, dominated by long wave radiation to space, occupy much of the middle and upper troposphere. The rate of change of entropy, s, per unit mass is given by $\frac{ds}{dt} = Q/T.$ The spatial distribution of entropy generation is similar to the spatial pattern of Q, as illustrated in Fig. 9.

Diabatic heating includes contributions from radiative heating and cooling, release of latent heat associated with phase transitions, heating by conduction of sensible heat, and heating by frictional dissipation:

$$Q = -\frac{1}{\rho} \{ \nabla \cdot F_{rad} + \rho L(e - c) + \nabla \cdot J_H + \tau : \nabla \vec{v} \}$$
 (6)

where ρ is the density of air, L is the latent heat of condensation, c and e are the rates of condensation and evaporation per unit mass, F_{rad} is the net radiative flux, J_H is the sensible heat flux due to conduction, τ is the wind tress tensor, and \vec{v} is the wind velocity.

The diabatic heating term Q can be written as $Q = Q_h + Q_f$, where Q_h accounts for radiative heating (solar and infrared), latent heating and heating due to conduction:

$$Q_h = -\frac{1}{\rho} \{ \nabla \cdot F_{rad} + \rho L(e - c) + \nabla \cdot J_H \}$$
 (7)

The second component, Q_f , is associated with frictional dissipation:

$$Q_f = -\frac{1}{\rho} \cdot \tau : \nabla \vec{v} \tag{8}$$

By separating Q_h from Q, we may consider Q_h as the external heating responsible, from a thermodynamic perspective, for the motion of the dry air. In the long run, the globally integrated values for Q_f must be balanced by global production of kinetic energy, equal therefore to $2.46 \ W/m^2$. Consequently, we may rewrite the generation of entropy as:

$$\frac{ds}{dt} = \frac{ds_h}{dt} + \frac{ds_f}{dt} \tag{9}$$

- where $\frac{ds_h}{dt} = Q_h/T$, $\frac{ds_f}{dt} = Q_f/T$ and T is the temperature of the environment in the region
- where heat is either absorbed or released [33, 34].
- In the long run, the entropy S of the entire atmosphere must remain constant. Thus, with
- 223 the long term mean indicated by " ":

$$\int_{alobal} \overline{\rho \frac{ds_h}{dt}} dV + \int_{alobal} \overline{\rho \frac{ds_f}{dt}} dV = 0$$
 (10)

225 or

$$\int_{global} \overline{\rho \frac{Q_h}{T}} dV + \int_{global} \overline{\rho \frac{Q_f}{T}} dV = 0$$
 (11)

- Since Q_f and T are always positive, the second term $\int_{global} \overline{\rho} \, \frac{\overline{Q_f}}{T} \, dV$ representing the entropy generation associated with dissipation is greater than zero, which implies that $\int_{global} \rho(\frac{Q_h}{T}) \, dV < 0$. It follows that the Q_h and T fields must be positively correlated. In other words, the general circulation can be maintained against the disordering impact of friction only if the heating occurs in warmer regions of the atmosphere with cooling in colder regions. Fig. 10 summarizes the creation and dissipation of kinetic energy in the atmosphere from a thermodynamic perspective.
- The global heat source Q_{in} in Fig. 10 represents the heat that the atmosphere absorbs at the higher temperature, T_{hot} , environment in order to do mechanical work. It is defined as $\int_{Q_h>0} \rho Q_h dV$. The global heat sink Q_{out} in Fig. 10 represents the heat that the atmosphere
- 237 releases into the lower temperature, T_{cold} , environment and is defined by $Q_{out} =$
- 238 $\int_{Q_h < 0} \rho Q_h dV.$

The mechanical work produced by the atmosphere is dissipated by friction and converted to heat that is released back into the atmosphere. This process is thermally equivalent to using the mechanical work to turn on a heater and return the exhausted heat back to the atmosphere, as depicted in Fig. 10. However, it is difficult to distinguish between Q_h and Q_f , and the absolute value of the global integral of Q_f is negligible compared to the global integral for Q_{in} and Q_{out} . Thus, the global heat source Q_{in} can be approximated as: $Q_{in} \approx \int_{Q>0} \rho Q dV$ with Q_{out} approximated as: $Q_{out} \approx \int_{Q<0} \rho Q dV$.

The value for the global heat source $\int_{Q>0} \rho Q dV$ averaged over the past three decades is estimated at 244 W/m^2 . The average kinetic energy production rate over the same period is calculated as 2.46 W/m^2 . It follows that the average efficiency for kinetic energy production is equal to approximately 1%.

The effective temperature $\langle T_{hot} \rangle$ at which heat is absorbed can be calculated as:

$$\langle T_{hot} \rangle = \frac{1}{\Delta S} \int_{t_1}^{t_2} \int_{Q_h > 0} T \frac{dS}{dt} dV dt \tag{12}$$

or approximated as:

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$$\langle T_{hot} \rangle \approx \frac{1}{\Delta S} \int_{t_1}^{t_2} \int_{Q>0} T \frac{dS}{dt} dV dt \tag{13}$$

where $\Delta S = \int_{t_1}^{t_2} \int_{Q_h > 0} \frac{dS}{dt} dV dt$, with t_1 and t_2 representing the starting and ending times for the integration. In the long run, the entropy S of the entire atmosphere is required to remain constant. Equation (10) can be recast as:

$$\frac{Q_{in}}{\langle T_{hot} \rangle} - \frac{Q_{out}}{\langle T_{cold} \rangle} + \frac{C}{T_{surface}} = 0 \tag{14}$$

where $\frac{C}{T_{surface}}$ represents the entropy generation due to dissipation [34]. The effective

temperature $\langle T_{cold} \rangle$ at which heat is released can be estimated accordingly.

The schematic illustration of the dry air component of the atmosphere as a thermal engine is summarized in Fig. 11, with values included here representing averages for the past 32 years. The dry air component of the atmosphere acts as a thermal engine, absorbing heat at a temperature of approximately 256K, releasing heat at a temperature of approximately 252K. The process produces kinetic energy at a rate of $2.46 W/m^2$ sustaining thus the circulation of the atmosphere against friction.

7. Discussion and summary

The study started with a quantification of the total kinetic energy stock of the atmosphere and subsequently investigated how kinetic energy is generated and dissipated from mechanical and thermodynamic perspectives.

The total kinetic energy stock of the atmosphere displays significant inter-annual variability, as indicated in Fig. 1 and Fig. 2, with the changing phases of the ENSO cycle playing an important role. This inter-annual variation reflects the fact that the wind energy potential for a particular location can fluctuate on a long-term basis, under the influences of long-term atmospheric oscillations which can alter the circulation of the atmosphere including the distribution of kinetic energy.

To illustrate the inter-annual variation of wind energy potentials, we select two locations, one in Texas (34.5 °N, 101.3 °W) and the other in North Dakota (47 °N, 101.3 °W), as indicated in Fig 12a. In calculating the potential electricity generated from wind, we chose to use power curves and technical parameters for the GE 2.5 MW turbines (rated wind speed 12.0 m/s, cut-in wind speed 3.5 m/s, and cut-out speed 25.0 m/s). The power curve of the wind turbine defines the

variation of power output as a function of wind speed. The hourly wind speeds at 100 m are extrapolated from winds at 50 m according to the relation: $V_{100} = V_{50} \cdot \frac{ln(Z_{100}/Z_0)}{ln(Z_{50}/Z_0)}$, where V_{100} and V_{50} indicate hourly values for the wind speed at 100 m and 50 m respectively, Z_{100} and Z_{50} define the elevation of the turbine hub (100 m) and the reference 50 m altitude, and Z_0 defines the surface roughness length.

The capacity factor (CF) values in Fig. 12b, at a particular time t_0 , are calculated as:

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$$CF(t_0) = \left(\int_{t_0 - 0.5 \ year}^{t_0 + 0.5 \ year} P_{real}(t) \cdot dt \right) / (P_{rated} \cdot 1year)$$
 (15)

where P_{real} denotes the power actually realized, and P_{rated} refers to the power that could have been realized had conditions permitted the turbine to operate at its name plate capacity. The seasonality of wind energy potentials, represent by CF values, have been removed due to the averaging period defined in equation (15): averaging P_{real} from $t_0 - 0.5$ year to $t_0 + 0.5$ year. CF values of the wind farms in Texas and North Dakota display significant interanual variation. The ups and downs of CF values in Fig 12b are the embodiments of the long-term atmospheric oscillations. Modern wind turbines are designed to work with an anticipated lifespan of 20 years. Wind energy potentials, as exemplified by the Texas and North Dakota cases, can vary on a year-to-year basis with a large amplitude over a 20 years period. Predictions of wind power for the next 20 years, or at least limits on its possible variation, will pose an important challenge for prospective investors in wind power.

The kinetic energy of wind in the atmosphere is constantly dissipated by friction. The residence time of kinetic energy, τ , is estimated at 6.9 days. The dry air component of the atmosphere generates kinetic energy as a thermal engine to sustain the general circulation of the atmosphere

against frictional dissipation. Key thermodynamic properties were quantified, including the kinetic energy production rate, C, the heat absorption rate, Q_{in} , the effective temperature at which heat is absorbed, $\langle T_{hot} \rangle$, and the effective temperature at which heat is released, $\langle T_{cold} \rangle$.

The calculations of these key properties are based on the assimilated meteorological data from the MERRA compilation. Data assimilation is the process of incorporating historical observations of the atmosphere into a numerical physical model, and produces the most reliable estimate of the past meteorological conditions. However, some uncertainties with the final outputs, such as wind speed data, cannot be completely eliminated.

The kinetic energy production rate, C, is calculated from a mechanical perspective using wind speed data and pressure gradient data. Wind speed data and pressure data are accurately obtained in the assimilation process [24]. Thus, the kinetic energy production quantified here is reliable, and the results obtained are consistent with other studies [18-22]. The quantification of other variables, notably diabatic heating and effective temperatures, involves parameters such as the vertical velocity of the air with relatively large uncertainties [24]. Absolute values of these thermodynamic properties are subject to relatively large uncertainty, depending as they do on the accuracy of the input data, the MERRA analysis in the case. It is not possible to place error bars on the values derived here for these parameters.

The globally averaged combined land and ocean surface temperature data indicate a warming of 0.85 K, over the period 1880 to 2012 [35]. A number of studies argued that the warming climate over the past decades has influenced the wind resource potential [36-44]. The upward trend in kinetic energy production rate obtained here confirms the fact that the thermodynamic conditions of the atmosphere have undergone a significant change over the past 32 years. A key question is

whether the conclusions reached in the study may be conditioned by the use of a specific data base. Other datasets including NCEP-1, NCEP-2, ERA-40 and JRA-25 should be employed in future to compare with results from the present study. Regarding the future warming climate, according to the IPCC 2014 report [35], the change in global surface temperature by the end of the 21st century is likely to exceed 1.5°C relative to the average from year 1850 to 1900 under most future greenhouse emission scenarios. It is essential to investigate how the atmosphere, as a thermal engine, will adjust under the different scenarios, altering thus the distributions and values of wind energy resources.

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A number of studies have suggested that large scale deployment of wind farms could potentially influence the circulation of the atmosphere [9, 11-16, 45-49]. With a simple parameterization of turbine operations, Miller et al. [46] performed numerical experiments and found that a maximum of 34 TW of electricity could be generated. Marvel et al. [47] extended Miller's work by parameterizing the turbines as sinks for momentum and concluded that wind turbines placed at the Earth's surface could extract kinetic energy at a rate of at least 400 TW, whereas highaltitude wind turbines could extract more than 1,800 TW. With a different global model and parameterization approach, Jacobson and Archer [48] argued that as the number of wind turbines increases over large geographic regions, power extraction would first increase linearly, then converge to a saturation limit, with a saturation potential in excess of 250 TW at 100 m globally, 380 TW at 10 km. There is a notable discrepancy between these various estimates. Adams and Keith [16] addressed the question using a mesoscale model. They concluded that wind power production would be limited to about 1 W/m² at wind farm scales larger than about 100 km² and that the mesoscale model results are quantitatively consistent with results from global models that simulated the climate response to much larger wind power capacities. However, as noted

earlier, the energetics of the entire atmosphere is different from the energetics of the mesoscale region.

The quantity of wind energy that can be extracted from the atmosphere to generate electricity depends ultimately on the rate at which kinetic energy is produced, not on the quantity of kinetic energy stored in the atmosphere [50]. Answering the question of the ultimate limit of the atmosphere as a source of wind-generated electric power requires a detailed study of the underlying thermodynamics of the global atmosphere. While not trying to quantify the ultimate wind potential, this study provides an analytical framework that can be adapted for future studies addressing the ultimate wind energy potential and the potential perturbations to the atmospheric circulation that could arise as a result of significant exploitation of this potential. It will be critical to understand how the key thermodynamic variables, such as the effective temperature $(T_{hot}$ and $T_{cold})$ and diabatic heating $(Q_{in}$ and $Q_{out})$, evolve as increasing numbers of large scale wind farms are deployed.

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486 Figures

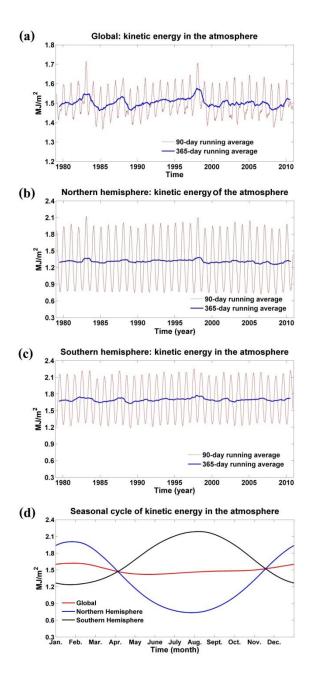


Fig. 1. (a) Variation of the global kinetic energy from January 1979 to December 2010. (b) Variation of the Northern Hemisphere kinetic energy from January 1979 to December 2010. (c) Variation of the Southern Hemisphere kinetic energy from January 1979 to December 2010. (d) The composite seasonal cycle of the kinetic energy of the atmosphere averaged over the past 32 years.

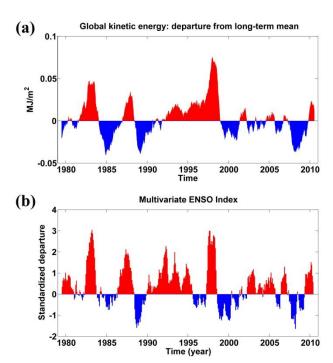


Fig. 2. (a) The departure of global kinetic energy from its 32 years' mean value $1.50 \, MJ/m^2$. The seasonality of the departure is removed via 365-day running average. (b) The time series of the multivariate ENSO index from January 1979 to December 2010. Positive values correspond to the warm events of the ENSO phenomena, while the negative ones correspond to the cold events.

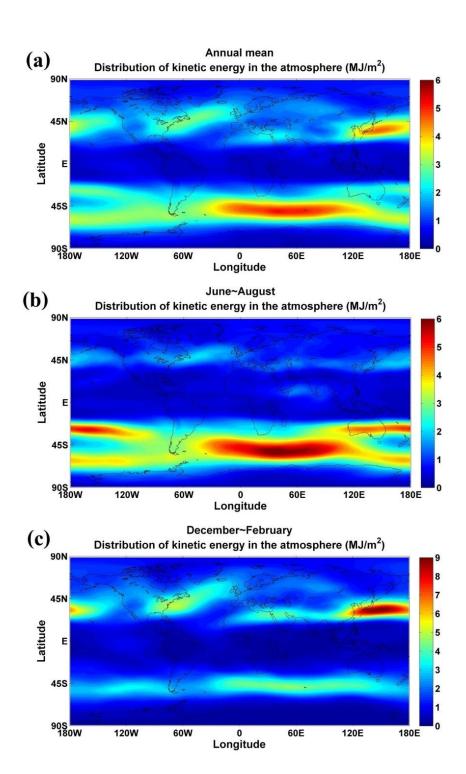


Fig. 3. (a) Spatial distribution of the annual mean kinetic energy of the atmosphere in MJ/m^2 , calculated based the past 32 years' data. (b) June ~ August, calculated based the past 32 years' data. (c) December ~ February, based on the past 32 years' data.

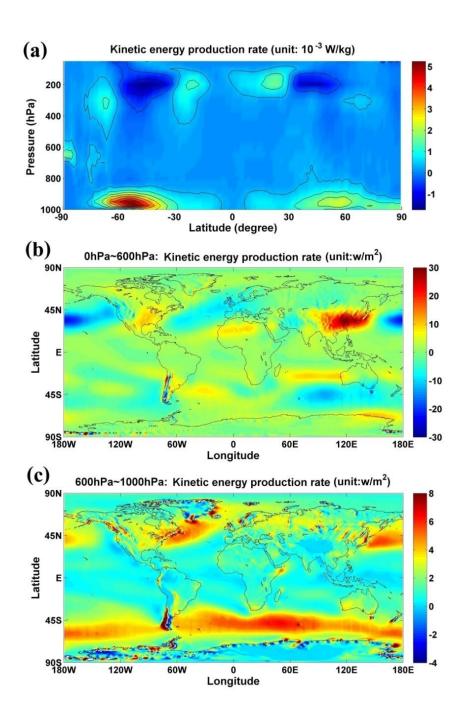


Fig. 4. (a) The vertical profile of kinetic energy production rate, C. (b) Kinetic energy production rate, C, in the layer between $0 \, hPa \sim 600 \, hPa$. (c) Kinetic energy production rate, C, in the layer between $600 \, hPa \sim 1000 \, hPa$.

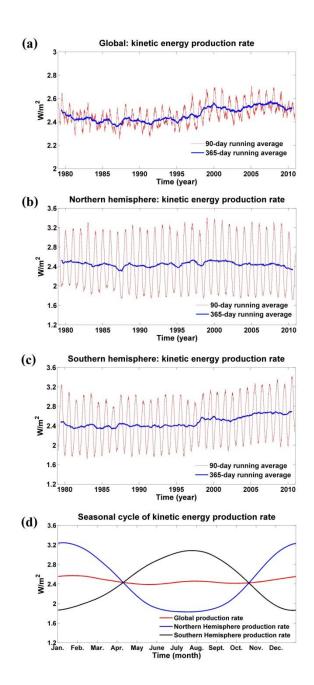


Fig. 5. (a) Variation of the global kinetic energy production rate, C, from January 1979 to December 2010. (b) Variation of the Northern Hemisphere kinetic energy production trend, C, from January 1979 to December 2010. (c) Variation of the Southern Hemisphere kinetic energy production trend, C, from January 1979 to December 2010. (d) The composite seasonal cycle of the kinetic energy production rate, C, based on the past 32 years' data.

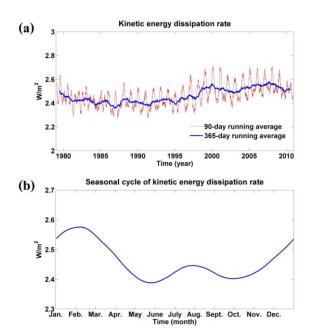


Fig. 6. (a) Variation of kinetic energy dissipation rate, *D*, from January 1979 to December 2010; (b) The composite seasonal cycle based on the past 32 years.

$$C = 2.46 \text{ W/m}^2$$

$$1.50 \text{ MJ/m}^2$$

$$D = 2.46 \text{ W/m}^2$$

Fig. 7. Mechanical perspective on the budget of atmospheric kinetic energy.

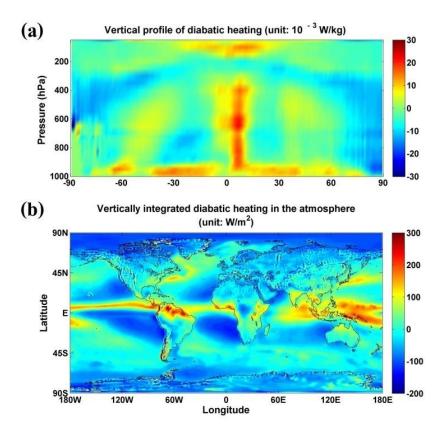


Fig. 8. (a) Vertical profile of diabatic heating. (b) Vertically integrated results.

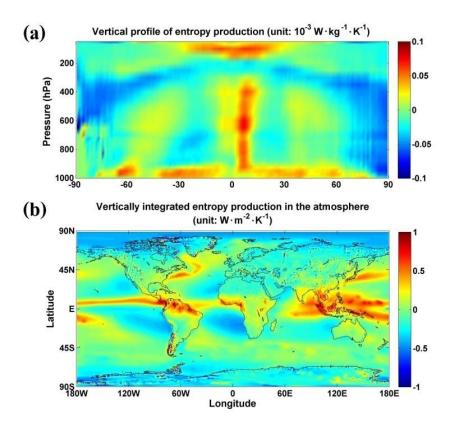


Fig. 9. (a) Vertical profile of entropy production. (b) Vertically integrated results.

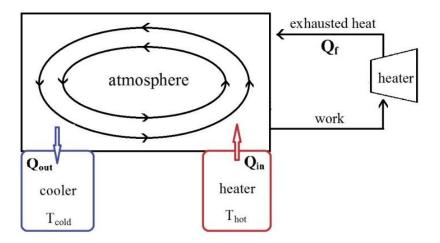


Fig. 10. Schematic depiction of the atmosphere as a thermal engine.

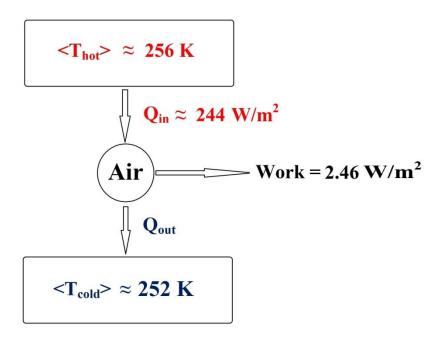


Fig. 11. Illustration of the atmosphere as a Carnot engine. Work, C, is dissipated ultimately by friction.

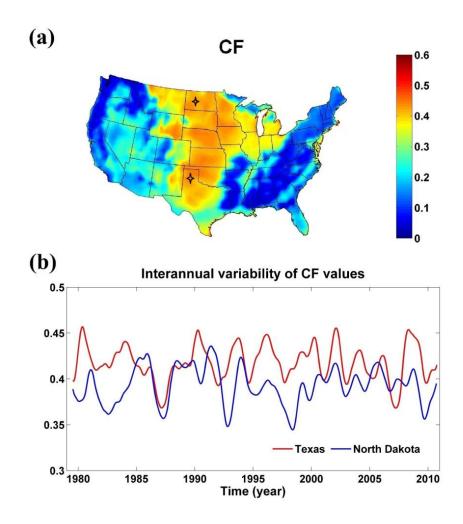


Fig. 12. (a) Color coded values for CF as a function of position averaged over the 32 year period Jan 1st 1979 to Dec 30th 2013. Positions of two wind farms considered in this paper are indicated by the stars. (b) CF values for two wind farms in Texas and North Dakota with seasonal cycle removed.