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A moisture-stratiform instability for convectively coupled waves

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Abstract

A simple model of two vertical modes is constructed and analyzed to reveal the basic instability mechanisms of convectively coupled waves. The main novelty of this model is a convective parameterization based on the quasi-equilibrium concept and simplified for a model of two vertical modes. It hypothesizes 1) approximate invariance of the difference between saturation moist static energy in the lower half of the troposphere and moist static energy in the sub-cloud layer, regardless of free troposphere humidity, 2) variations in the depth of convection is determined by moisture deficit variations in the mid-troposphere. Physical arguments for such a treatment are presented. For realistic model parameters chosen based on cloud system resolving model simulations (CSRM) of an earlier study, the model produces unstable waves at wavelengths and with structures that compare well with the CSRM simulations and observations.

A moisture-stratiform instability and a direct stratiform instability are identified as the main instability mechanisms in the model. The former relies on the effect of midtroposphere humidity on the depth of convection. The latter relies on the climatological mean convective heating profile being top heavy, and is identified to be the same as the stratiform instability mechanism proposed by Mapes (2000). The moisture-stratiform instability appears to be the main instability mechanism for the convectively couple wave development in the CSRM simulations. The finite response time of convection has a damping effect on the waves that is stronger at high wavenumbers. The net moistening effect of the second mode convective heating also damps the waves, but more strongly at low wavenumbers. These effects help to shape the growth rate curve so that the most unstable waves are of a few thousand kilometers in scale.

1. Introduction

There is a long history of constructing models with gross vertical structures to capture the basic dynamics of convectively coupled tropical waves (e.g. Lindzen, 1974; Emanuel, 1987; Neelin et al., 1987; Wang, 1988; Mapes, 2000; Majda and Shefter, 2001; Khouider and Majda, 2006). Earlier models emphasized a first baroclinic structure (or mode) that is of one sign over the full depth of the free troposphere (e.g. Lindzen, 1974; Emanuel, 1987; Neelin et al., 1987; Wang, 1988). More recent observations of these waves revealed a significant second baroclinic component in their vertical temperature structures (e.g. Wheeler et al., 2000; Straub and Kiladis, 2002; Haertel and Kiladis, 2004). Such observations alone do not contradict models based only on the first baroclinic mode; it is possible that the first baroclinic mode captures the basic dynamics and the second mode temperature structure is simply a byproduct. The more convincing evidence for the inadequacy of the first baroclinic mode models is that they do not yield instability without external destabilization mechanisms (Emanuel et al., 1994), which is inconsistent with the results of cloud system resolving model (CSRM) simulations (e.g. Tulich et al., 2006:Kuang, 2007). Mapes (2000) proposed the first instability model that contains both the first and the second baroclinic modes, and identified a stratiform instability for the wave-convection coupling (Mapes, 2000), hereafter M00. The behavior of such models has been analyzed in some detail (Mapes, 2000; Majda and Shefter, 2001; Majda et al., 2004). In these models, modulation of convection by the second mode temperature anomaly is emphasized, and effects of free troposphere moisture variations are ignored. Results from Kuang (2007), hereafter K07, however, indicate that moisture is an essential component for allowing convectively coupled waves to develop. Moisture was included

in the two vertical mode model of Khouider and Majda, (2006a), hereafter KM06, along with a third cloud type, congestus (in addition to the deep convective and stratiform clouds in M00). While considerable analyses have been done on the linear stability of this model (KM06; Khouider and Majda, 2006b), its convective parameterization is rather complicated and an instability mechanism involving moisture was not clearly identified.

This study continues the effort to construct models of convectively coupled waves with crude vertical structures. Our emphasis will be on conceptually simple convective parameterizations and on revealing the model's basic instability mechanisms. The model formulation is presented in section 2, along with results from linear analyses. The model parameters are selected based on CSRM simulations of convectively coupled waves described in K07 so that the model resides in realistic parameter regimes (Appendix A). The model is then simplified further and limiting cases are considered to reveal its basic instability mechanisms (section 3). This is followed by a summary and discussion section (section 4) and three appendices.

2. Formulation and linear analyses of the simple model

Like earlier models (e.g. M00; Majda and Shefter, 2001, hereafter MS01; KM06), the present model has two components: the first describes the response to convective heating and the second describes the convective parameterization.

a. Response to convective heating

Similar to K07, we start with the linear inviscid anelastic 2D primitive equations for a horizontal wavenumber k with a background state of no motion, and eliminate pressure and horizontal winds. This gives

$$\left(\frac{\partial}{\partial t} + \varepsilon\right) \left(\bar{\rho}w'\right)_{zz} = -k^2 \bar{\rho}g \frac{T'}{\bar{T}}$$

$$\frac{\partial}{\partial t}T' + w' \left(\frac{d\bar{T}}{dz} + \frac{g}{c_p}\right) = J'$$
(1)

where ε is the mechanical damping coefficient, taken to be a constant, J is convective heating, and all other symbols assume their usual meteorological meaning. The overbar denotes the background mean variables and prime denotes deviations from the mean. Despite the various assumptions and simplifications, systems such as Eq. (1) capture well the basic wind and temperature distributions of convectively coupled waves given the convective heating and cooling. This was shown for the 2-day waves (Haertel and Kiladis, 2004) and is true for the present case as well (not shown).

We then assume rigid plate boundary conditions at the surface and at the top of the troposphere and expand the forcing and the solution in terms of the vertical eigenmodes (G_i):

$$\overline{\rho}w'\left(\frac{d\overline{T}}{dz} + \frac{g}{c_p}\right) = \sum_{j=1}^2 w_j(x,t)G_j(z)\left(\frac{d\overline{T}}{dz} + \frac{g}{c_p}\right)$$

$$\overline{\rho}T' = \sum_{j=1}^2 T_j(x,t)G_j(z)\left(\frac{d\overline{T}}{dz} + \frac{g}{c_p}\right)$$

$$\overline{\rho}J' = \sum_{j=1}^2 J_j(x,t)G_j(z)\left(\frac{d\overline{T}}{dz} + \frac{g}{c_p}\right)$$
(2)

and obtain:

$$\left(\frac{\partial}{\partial t} + \varepsilon\right) w_j - k^2 c_j^2 T_j = 0$$

$$\frac{\partial}{\partial t} T_j + w_j = J_j$$
(3)

Without forcing and damping, the solutions to Eq. (3) for each vertical mode are two neutral waves propagating in opposite directions with a dry wave speed of c_i . When the

buoyancy frequency, the square of which is $N^2 = g\left(\frac{d\ln\overline{T}}{dz} + \frac{g}{c_p\overline{T}}\right)$, is constant, the

vertical modes are

$$G_{j}(z) = \frac{\pi}{2} \sin\left(\frac{j\pi z}{H_{T}}\right)$$
(4)

where H_T is the height of the troposphere. The modes are normalized so that their absolute values average to unity over the depth of the troposphere. We have retained only the first two vertical modes with the goal of constructing a minimal model to reveal the basic instability mechanisms. Note that congestus and stratiform heating are treated here as opposite phases of the same mode (J₂). This simpler treatment represents the observed and CSRM simulated heating structures very well (Haertel and Kiladis, 2004; K07).

It is useful to remind ourselves the empirical nature of the two-mode model: the two vertical modes are chosen not because they are mathematically the first two eigenmodes of Eq. 1 with the rigid plate boundary conditions. They are chosen because of the empirical evidence that basic vertical structure of the waves can be captured with these two modes (e.g. Haertel and Kiladis, 2004; K07). Indeed, it is based on this empirical evidence and the evidence that a radiation upper boundary condition does not have a major effect on the wave characteristics (K07) that the rigid plate boundary conditions were then chosen, allowing Eq. 1 to be conveniently decomposed into vertical modes that resemble the vertical modes seen empirically. Therefore, the present model does not address why these particular vertical structures/modes dominate, the answer to which requires a model that allows vertical modes to be selected naturally.

Eq (3) is augmented by an equation for the subcloud layer moist static energy h_b and an equation for the mid-tropospheric humidity q_{mid} . The equation for h_b follows prior studies (e.g. M00, MS01, KM06):

$$\frac{\partial h_b}{\partial t} = E - b_1 J_1 - b_2 J_2 \tag{5}$$

where E is the tendency from surface heat flux anomalies, and b_1 and b_2 represent the reduction of h_b per unit J_1 and J_2 , respectively. In reality, large-scale vertical advection has a smaller but non-negligible effect on h_b , although including them does not appear to change the basic behaviors of the model so they are left out for simplicity. In this paper, we further set E=0 to eliminate any surface heat flux feedbacks, which, as shown in K07, do not change the basic characteristics of the waves.

The equation for q_{mid} can be written as:

$$\frac{\partial q_{mid}}{\partial t} = a_1 w_1 + a_2 w_2 - d_1 J_1 - d_2 J_2 \tag{6}$$

where a_1 and a_2 represent the effective moisture stratification for the two modes, d_1 and d_2 represent the convective drying effect on q_{mid} per unit J_1 and J_2 . We have neglected horizontal advection of moisture. The parameters a_1 and a_2 can be derived given the background moisture stratification and the vertical structure of w_1 and w_2 . In KM06, vertically averaged free troposphere humidity <q> was used in Eq. (6) so that column moist static energy conservation can be used to constrain d_1 and d_2 . However, the main purpose of including an equation for moisture is to include the role of tropospheric

humidity on convection, as discussed in more detail in section 2b. While conveniently constrained by column moist static energy conservation, <q> is not necessarily the most relevant quantity for this purpose, even though it could serve as a reasonable approximation. In this paper, we will use the mid-tropospheric humidity q_{mid} instead, and forgo the convenience of using <q>.

As discussed further in Appendix A and noted in many previous studies (e.g. Haertel and Kiladis, 2004), there is substantial compensation between adiabatic cooling and convective heating associated with the first mode, i.e. $w_1 \sim J_1$. Furthermore, because q_{mid} is located around the nodal point of w_2 , the effect of large-scale advection by w_2 on q_{mid} (i.e. a_2) is small. We may therefore simplify Eq. (6) to

$$\frac{\partial q_{mid}}{\partial t} = m_1 J_1 + m_2 J_2 \tag{7}$$

where $m_1 \approx a_1 - d_1$ and $m_2 \approx -d_2$ are the moistening effects per unit J_1 and J_2 . We have again verified that this simplification does not modify the basic behaviors of the model discussed in this paper.

Equations (3), (5), and (7) describe the atmosphere's response to convective heating. We non-dimensionalize the above equations using the first dry baroclinic gravity wave speed (50m/s) as the velocity scale so that c_1 is 1, and c_2 is set to $\frac{1}{2}$. We use 1 day as the time scale, so the length scale is 4320km, and T_j , h_b , and q are expressed in temperature unit¹ (1K) so that the scale for J_j and w_j is 1K/day.

 $^{^{1}}$ q is expressed in Kelvin by dividing the associated latent energy by the specific heat. The same applies to saturation humidity q* below.

The dry dynamics are similar to those used in previous studies, e.g. M00, MS01, KM06. The main new feature of this model is its convective parameterizations that determine J_1 and J_2 , described below.

b) Convective parameterizations

First, we define an integrated upper tropospheric heating anomaly U (scaled by the depth of the troposphere)

$$U = (J_1 - J_2) / 2 \tag{8}$$

and an integrated lower tropospheric heating anomaly L

$$L = (J_1 + J_2)/2$$
 (9)

and assume that in statistical equilibrium, the ratio of the total upper tropospheric heating (mean plus anomaly) to the total lower tropospheric heating is related to the anomalous moisture deficit (relative to saturation) in the mid-troposphere by

$$\frac{U+U_0}{L+L_0} = r_0 + \frac{r_q}{L_0} q^+$$
(10)

where the subscript 0 denotes background mean values, and $U_0=r_0L_0$, and a negative q^+ indicates anomalous moisture deficit. In the mid-troposphere (say, 500hPa and 270K), upon expressing the saturation humidity q^* in units of Kelvin, we have $\partial q^*/\partial T \sim 1$. Further taking into account the fact that the first mode is near its peak value ($\pi/2$) in the midtroposphere, we have

$$q^{+} = q_{mid} - \frac{\pi}{2} T_1 \left(\frac{\partial q^*}{\partial T} \right)_{midtrop}$$

$$\approx q_{mid} - 1.5 T_1$$
(11)

Eq. (10) states that for the same amount of convection in the lower troposphere, there is less convection in the upper troposphere when the mid-troposphere is dry. The notion that a dry mid-troposphere limits the depth of tropical convection is well supported by observations, numerical simulations, and theoretical reasoning (Brown and Zhang, 1997;Sherwood, 1999;Parsons et al., 2000;Redelsperger et al., 2002;Ridout, 2002;Derbyshire et al., 2004;Takemi et al., 2004;Roca et al., 2005;Kuang and Bretherton, 2006). One plausible interpretation (e.g. Brown and Zhang, 1997; Derbyshire et al. 2004; Kuang and Bretherton, 2006) is that all else being equal, with a dry mid-troposphere, convection does not reach as high because entrainment of drier environmental air by the rising air parcels leads to more evaporative cooling, and hence negative buoyancy. More detailed studies, however, are needed to place this interpretation on a firmer footing. Moisture deficit, or saturation deficit, has been used as a control on convection before (Raymond, 2000), except in terms of precipitation instead of the height of convection.

We shall consider the adjustment of the U/L ratio (denoted as r) to moisture deficit to be instantaneous. One could take into consideration the finite response time of r so that:

$$\frac{\partial r}{\partial t} = \tau_r^{-1} \left(r_{eq} - r \right) \tag{12}$$

where r_{eq} is the ratio anomaly that is in statistical equilibrium with its large-scale environment (Eq. (10)) and τ_r is the adjustment time for r to approach that equilibrium. We consider τ_r to be of the same order as the time for convective updrafts to rise from the lower troposphere to the upper troposphere (hours or less). For τ_r values in this range, inclusion of this adjustment process does not change the basic behavior of the model so we will leave it out in this paper. Note that τ_r is not the relaxation time for moisture anomalies, which will be discussed in section 3 and is on the order of a day.

Second, we consider that saturation moist static energy averaged over a layer above the cloud base is in quasi-statistical equilibrium (QE) with the subcloud layer moist static energy. When the equilibrium is achieved instantaneously, we have

$$\frac{\partial h_b}{\partial t} = \left\langle \frac{\partial h^*}{\partial t} \right\rangle \tag{13}$$

The bracket on the right hand side denotes averaging over a layer above the cloud base. The variable h^* is the saturation moist static energy. We then rewrite Eq. (13) as

$$\frac{\partial h_b}{\partial t} = F \frac{\partial}{\partial t} \left[fT_1 + (1 - f)T_2 \right]$$
(14)

where $F=\partial h^*/\partial T$. The factors f and (1-f) are the relative weights of T_1 and T_2 . We shall interpret f as measuring the importance of undiluted parcels in the total convective mass flux. An f close to 1 implies that the convective mass flux is dominated by undiluted parcels, and Eq. (13) holds with <h*> taken as an average over the whole troposphere. In this case, the approximate invariance of convective available potential energy (CAPE) is effectively used as a simplification for QE over the whole depth of the troposphere, as in e.g. Emanuel et al. (1994). An f close to 0 implies that the convective mass flux is dominated by heavily entraining parcels, and Eq. (13) holds with <h*> averaged over a shallow layer above the cloud base. In this case, Eq. (14) effectively assumes convective inhibition (CIN) (within the two-vertical mode framework) to be approximately invariant. This is known as the boundary layer quasi-equilibrium (BLQ) (Emanuel, 1995;Raymond, 1995). Our normative value for f is 0.5 where <h*> may be viewed as an average over the lower half of the troposphere. To emphasize the instantaneous adjustment, we will refer to Eq. (14) (or Eq. (13)) as strict quasi-equilibrium (SQE), following Emanuel et al. (1994), where the word "strict" simply means that the adjustment is instantaneous.

For a given U/L ratio, we plug Eqs. (3) and (5) into Eq. (14) and make use of Eqs. (8), (9), and (10) to solve for the lower tropospheric heating in SQE, denoted as L_{eq}:

$$L_{eq} = B^{-1} \Big[Ar_q q^+ + f w_1 + (1 - f) w_2 \Big]$$
(15)

where

$$q^{+} \equiv q - 1.5T_{1}$$

$$A \equiv 1 - 2f + \frac{b_{2} - b_{1}}{F}$$

$$B \equiv 1 + \frac{b_{2} + b_{1}}{F} - Ar_{0}$$
(16)

Eq. (15) is a straightforward restatement of the SQE condition of Eq. (14), and the various terms have clear physical meanings: provided that A and B are positive, uplifting in the lower troposphere or a moist mid-troposphere increases convective heating in the lower troposphere in SQE. L_{eq} can also be expressed in terms of $\partial T/\partial t$. This form will be used in section 3. In Eq. (16) and for the rest of the paper, we omit the subscript in q_{mid} to simplify the notation. Taking into consideration the finite adjustment time to achieve QE, denoted as τ_L , we have:

$$\frac{\partial L}{\partial t} = \tau_L^{-1} \left(L_{eq} - L \right) \tag{17}$$

We expect τ_L to be on the order of a few hours, the time for a few turnovers of shallow cumulus convection. From L and the U/L ratio, J₁ and J₂ can be easily determined, completing our convective parameterization.

The present convective parameterization falls within the QE framework first introduced by Arakawa and Schubert (1974), which states that convection should be in a state of statistical equilibrium with the large-scale flow. In some previous simple models of the interaction between large-scale circulation and deep convection (e.g. Emanuel et al., 1994), the approximate invariance of convectively available potential energy (CAPE) is used as a simplification for SQE over the whole depth of the troposphere (i.e. f=1). As noted earlier, this emphasizes the role of undiluted parcels in deep convective mass flux, based on which CAPE is computed. Recent evidence, however, indicates that this is not a good simplification of SQE, at least in cases such as convectively coupled waves. Highresolution numerical studies show that undiluted parcels do not make a significant contribution to the overall convective mass flux (Khairoutdinov and Randall, 2006;Kuang and Bretherton, 2006). This is corroborated by the observed and simulated sensitivity of convection to tropospheric moisture (see discussion in relation to Eq. (10)).

In the present treatment, we are using the invariance of a shallow CAPE as a simplification of SQE over the lower half of the troposphere (with f=1/2 in Eq. (14)). The shallow CAPE measures the integrated buoyancy for undiluted parcels only up to the mid-troposphere. This is a simplification for the present simple model with only two vertical modes in the free troposphere. It by no means suggests that cloud parcels do not experience entrainment in the lower troposphere. However, the cumulative effect of entrainment is smaller in the lower troposphere because of the shorter distance traveled

by the cloud parcels and their smaller moist static energy difference from the environment (for the regions that we are concerned with, the lower troposphere is taken to be always sufficiently moist so that its moist static energy is close to that of the cloud parcels). Therefore, neglecting the effect of entrainment and using Eq. (14) is a reasonable simplification for SQE over the lower half of the troposphere. We then use Eq. (10) to explicitly include the effect of entrainment on the convective mass flux that can reach from the lower to the upper half of the troposphere. In Eq. (10), we have neglected the role of the traditional CAPE (defined for undiluted parcels over the whole depth of the free troposphere). This reflects the view that the mass flux reaching the upper troposphere is in significantly diluted updrafts, and mid-tropospheric moisture deficit is the dominating factor that controls the depth of convection (through entrainment). The CAPE anomalies can become important when they are sufficiently negative so that the background CAPE is substantially consumed, and is a nonlinearity that can limit the growth of the waves. Further discussions of nonlinearity, however, will not be presented in this paper.

c. Linearized equations and normative parameter values

The system is linearized by replacing Eq. (10) with

$$U = r_0 L + r_a q^+ \tag{18}$$

The linearized model thus consists of the prognostic equations (3), (6), and (17), and the auxiliary equations (8), (9), (15), and (18).

Observed and simulated data from, for example, K07 and Haertel and Kiladis (2004), may be used to estimate the parameters by viewing such data in the framework of the present model. This is discussed in Appendix A. Table 1 lists the normative parameter values used in the paper based on these estimates. It is important to stress that because of the highly simplified nature of the present model, viewing observations or the CSRM results in its framework is very approximate and the parameter estimates are only intended as educated guesses of plausible values.

d. Linear Analysis

Results from a linear analysis of this system are shown in Figure 1. Waves with wavelengths from 1500km to 40000km are unstable with a maximum growth rate of about 0.13/day at 5000km. The unstable waves have phase speeds around 20m/s, slightly slower than the dry wave speed of the second vertical mode. The eigenvector at a wavelength of 8640km is expressed in physical space in Figure 2a,b. The eigenvector is scaled so that T_1 is a sine function with amplitude of one. We have further reconstructed the vertical structure of temperature and convective heating (Figure 2c,d) so that it is visually more direct to compare with observations. We have used $sin(j\pi z/H_T)$, j=1,2 as the vertical structures with H_T=14km. These figures show that the linear model yields instability at wavelengths and with structures that compare well with the CSRM simulations and observations. Note that convective heating here is dominated by the first vertical mode and has a significant tilt, consistent with the observations/ simulations (Haretel and Kiladis, 2004; K07). In contrast, in the model of KM06, heating in the upper troposphere is substantially stronger than that in the lower troposphere (their Fig. 6). There is also a tendency for this to be true in MS01 as the wavelength increases to beyond 2000km (their Fig. 4). The substantially stronger heating in the upper troposphere indicates a larger contribution from the second mode heating and a more in-phase relation

between J_1 and $-J_2$, compared to Figure 2d. Figure 3 shows the phase lag between J_1 and $-J_2$ as a function of wavenumber. Substantial phase lag is seen at all wavenumbers. Over a wide range of wavelengths (from 1500km to 10000km), the phase lag is between ~85 to ~65 degrees. This is consistent with the CSRM simulation results from K07.

We have repeated the linear analysis with the parameters perturbed around their normative values one at a time. The parameter dependence of the maximum linear growth rate is shown in Figure 4. While not shown, the phase speeds of the most unstable modes are between 10 and 25m/s except with $b_1 < 0.6$, $b_2 > 3.3$, $d_1 < 0.9$, $d_2 > -0.6$, $a_1 > 1.6$, or $a_2 < -0.4$, where the phase speeds of the most unstable modes are a few m/s or less. While it is useful to know the parameter sensitivities of the model, for the purpose of revealing the basic instability mechanisms, it is more informative to consider certain limiting cases, as discussed in section 3.

It is useful to note that while r_q and f are separate parameters in the model and are varied independently in Figure 4, they are related to the conceptual picture of whether upper troposphere convective mass flux is dominated by nearly undiluted or significantly diluted updrafts. When significantly diluted updrafts dominate, the mid-troposphere humidity has an important effect on the depth of convection, and r_q will be large, f will be small (a smaller depth of the atmosphere can be assumed to be in QE regardless of the environment humidity). Thus one should in principle vary these parameters together to be conceptually consistent, although this is not done here.

3. The basic instability mechanisms

3.a A slightly simplified version of the model

To reveal its basic instability mechanisms, we make a few simplifications to the model described in section 2. First, we replace the two-way wave equations Eq. (3) with one-way wave equations with a Newtonian cooling coefficient ε :

$$\frac{\partial T_j}{\partial t} + c_j \frac{\partial T_j}{\partial x} = J_j - \varepsilon T_j$$
(19)

and use Eq.(7) instead of Eq.(6) to evolve mid-tropospheric humidity. Replacing the twoway wave equations by one-way wave equations has some quantitative effects, as discussed in Appendix B. For example, heating drives temperature anomalies more effectively in the one-way wave equations, and this effect is stronger for the first vertical mode. However, these changes do not alter the basic behavior of the model. It is also convenient to rewrite Eq.(18) in terms of J_1 and J_2 :

$$J_2 = \gamma_0 J_1 - \gamma_q q^+ \tag{20}$$

where

$$\gamma_{0} \equiv \frac{1 - r_{0}}{1 + r_{0}}$$

$$\gamma_{q} \equiv \frac{2r_{q}}{1 + r_{0}}$$
(21)

and include the finite adjustment time to achieve QE as:

$$\frac{\partial J_1}{\partial t} = \tau_J^{-1} \left(J_{1,eq} - J_1 \right) \tag{22}$$

where

$$J_{1,eq} = \frac{1}{b_1 + b_2 \gamma_0} \left\{ b_2 \gamma_q q^+ - F \frac{\partial}{\partial t} \left[fT_1 + (1 - f)T_2 \right] \right\}$$
(23)

Here, we have expressed $J_{1,eq}$ in terms of $\partial T/\partial t$, although one can also write it in a form similar to Eq. (15). We shall take $\tau_J = \tau_L$. Physically, it is perhaps more natural to apply the finite adjustment time on lower tropospheric heating L instead of J_1 , as L is more locally determined by the subcloud layer and the lower troposphere. However, since $J_1 = (1+r_0)L + r_q q^+$, the difference in relaxing J_1 instead of L lies in the $\partial q^+/\partial t$ term. Because τ_L is considerably shorter than the timescale for q^+ to vary (on the order of the wave period), Eq. (22) has the same basic effect as Eq. (17).

The phase speeds and the linear growth rates for this simplified version are shown in Figure 5 and the structures for a wavelength of 8640km are shown in Figure 6. The higher wavenumbers are more stable compared to Figure 1 and the amplitudes of J_1 and J_2 are smaller compared to those in Figure 2. The latter is because heating is more effective in driving temperature anomalies in one-way equations (Appendix B). When this difference is accounted for following discussion in Appendix B, the amplitudes of J₁ and J_2 become similar to those in Figure 2. We have also repeated the linear analysis with the parameters perturbed around their normative values one at a time for this simplified version of the model. The parameter dependence of the maximum linear growth rate is shown in Figure 7, and is similar to that in Figure 4 in terms of its basic pattern. The parameter dependence on m_1 and m_2 are shown instead of a_1 , a_2 , d_1 , and d_2 because Eq (7) is used. The dependence on ε is also similar to that in Figure 4 (not shown). Similar to the model in section 2, all unstable waves have phase speeds between 10 and 25m/s except with $b_1 < 0.6$, $b_2 > 10/3$, $m_1 > 0.5$, or $m_2 < 0.6$, where the phase speeds of the most unstable modes are a few m/s or less. This dependence is explained in section 3.b.2 and Appendix

C. The similarity in the basic parameter dependence indicates that the simplified system captures the basic behavior of the model described in section 2c.

In this paper, we focus on regimes with $m_1>0$. Moistening of the mid-troposphere by deep convection is clearly seen in K07. With $m_1>0$, the basic behavior of the system is preserved without including contribution of T_1 in q^+ so we will take $q^+=q$. The contribution of T_1 in q^+ has an important stabilizing role when $m_1<0$. This regime, however, is not the subject of this paper, and will not be discussed further.

3.b The regime with $\gamma_0 \ge 0$ and a moisture stratiform instability

We first consider the model behavior with $\gamma_0 \ge 0$ (i.e. $r_0 \le 1$), which corresponds to an atmosphere in which, climatologically speaking, the convective heating in the lower troposphere is greater than or equal to that in the upper troposphere. We shall try to identify the model's basic instabilities by considering limiting cases. To simplify the discussion, we take $b_2=0$ and $\gamma_0=0$. Physically, $b_2=0$ means that convection in the upper and lower troposphere have the same effect on h_b per unit heating and $\gamma_0=0$ means that the background convective heating is of the same strength in the upper and lower troposphere. These are not required but help to simplify our discussion. The results are largely representative of general cases with $\gamma_0 \ge 0$ and non-representative results will be pointed out along the way. Limiting cases with general parameter choices can be reduced to the same form by redefining the parameters as discussed in Appendix C.

3.b.1. Limiting case I: f=1

Let us first consider the limiting case with f=1 so that Eq. (23) reduces to

$$J_{1,eq} = -\frac{F}{b_1} \frac{\partial T_1}{\partial t}$$
(24)

Physically, this represents a case where convective mass flux is dominated by undiluted updrafts. In this case the sub-cloud layer moist static energy h_b is changed only by J_1 (as $b_2=0$) and is in equilibrium with T_1 alone (as f=1). Eq. (24) simply states that $J_{1,eq}$ is that required to keep $\partial h_b/\partial t$ the same as $F\partial T_1/\partial t$. In this case, the first mode (temperature and heating) is no longer affected by the second mode or moisture. This reduces the system to the first baroclinic mode model discussed in previous studies (Emanuel, 1987;Neelin et al., 1987). Let us start with $\varepsilon=0$ (no Newtonian cooling) and $\tau_J=0$ (i.e. in SQE), so that

$$\frac{\partial T_1}{\partial t} + c_1 \frac{\partial T_1}{\partial x} = -\frac{F}{b_1} \frac{\partial T_1}{\partial t}$$
(25)

The convectively coupled first vertical mode has a zero growth rate and a phase speed $c_1^*=c_1/(1+F/b_1)$ due to the reduced effective static stability. The first vertical mode also forces a response in T₂ and q (in a one-way interaction) through the effect of J₁ on J₂, both directly (Eq.(20)), and indirectly through J₁'s effect on moisture, and resonance occurs when $c_2=c_1^*$. The direct effect vanishes with $\gamma_0=0$, but does not with more general parameter choices. The temperature and heating structures for a simple case (b₂=0, $\gamma_0=0$, $\epsilon=0$, $\tau_J=0$, and m₂=0; other parameters take their normative values) are shown in Figure 8. The q field in this case is simply $-J_2/\gamma_q$. The phase speed c_1^* is 10m/s and the wave structures in many aspects resemble the observed patterns.

So far, the growth rate is 0 for all wavenumbers. Introducing a finite τ_J causes heating J₁ to lag T₁ by more than $\pi/2$ in phase, which gives rise to a damping effect that is stronger

at high wavenumbers. This has been pointed out before and was named moist convective damping (MCD) (Emanuel, 1993;Emanuel et al., 1994;Neelin and Yu, 1994;Yu and Neelin, 1994). A positive ε further damps the waves.

3.b.2. Limiting case II: f=0

Let us now consider f=0, corresponding to an atmosphere in which heavily entraining parcels dominate the convective mass flux. Here, the sub-cloud layer h_b is in equilibrium with T_2 alone, and there is no more dependence on T_1 of the other variables. Again, we take b_2 =0 and γ_0 =0 for simplicity. In this case, Eq. (23) reduces to

$$J_1 = -\frac{F}{b_1} \frac{\partial T_2}{\partial t}$$
(26)

i.e., J_1 is that required to keep $\partial h_b/\partial t$ the same as $F\partial T_2/\partial t$. First consider a system in SQE,

$$\frac{\partial T_2}{\partial t} + c_2 \frac{\partial T_2}{\partial x} = -\gamma_q q \tag{27}$$

$$\frac{\partial q}{\partial t} = -m_1 \frac{F}{b_1} \frac{\partial T_2}{\partial t} - m_2 \gamma_q q$$
(28)

where we have used $J_2 = -\gamma_q q$ (as $\gamma_0 = 0$). Assuming solutions of the form exp[i(kx- ω t)], we obtain the dispersion relationship

$$\boldsymbol{\omega}^{2} - \left[c_{2}k + i\gamma_{q}\left(\frac{Fm_{1}}{b_{1}} - m_{2}\right)\right]\boldsymbol{\omega} - im_{2}\gamma_{q}c_{2}k = 0$$
⁽²⁹⁾

Eqs. (27) and (28) describe a coupled system of T_2 and q. The effect of T_2 on q (through its effect on J₁ and, in turn, the moistening effect of J₁ on q, as expressed in Eq.(28)) coupled with the effect of q on T_2 (through its effect on J₂ and, in turn, the heating effect of J₂ on T₂, as expressed in Eq. (27)) give rise to an instability. This is best seen with m₂=0. Putting aside the less interesting solution ω =0, we have q=-(m₁F/b₁)T₂ and the heating J₂ is exactly in phase with T₂ and ω =c₂k+im₁ γ_q F/b₁, i.e. the phase speed is c₂ and the growth rate is m₁ γ_q F/b₁ at all wavelengths. The growth rate is proportional to m₁ γ_q , which measures how strongly the depth of convection depends on q (the factor γ_q) and how strongly moisture depends on J₁ (the factor m₁). It is also proportional to F/b₁, which measures how strongly J₁ depends on ∂ T₂/ ∂ t. While we have chosen b₂=0 and γ_0 =0 here, this picture holds for more general parameter choices as well (Appendix C), except the strict dependence on m₁, which is specific to the choice of b₂=0, γ_0 =0. For more general

parameter choices, a modified
$$m_1$$
, $\hat{m}_1 \equiv \frac{m_1 + m_2 \gamma_0}{1 + b_2 \gamma_0 / b_1}$, should be used (Appendix C).

In this limiting case, T_1 is forced by J_1 but does not feed back onto J_1 . The physical structure of the wave with a wavelength of 8640km from this limiting case in SQE is shown in Figure 9. The q field in this case is again simply $-J_2/\gamma_q$.

A positive m₂, which implies that the net effect of the second mode heating is to moisten the troposphere, brings a damping effect on q (Eq. (28)). The physical picture is simple: when, for instance, the troposphere is dry (q<0), convection is shallower (J₂>0); the combined effect of vertical advection and precipitation associated with the second mode heating moistens the atmosphere (i.e. m₂J₂>0), reducing the dry anomaly. That m₂ is positive should be expected based on observations: the effect of second mode vertical advection on mid-troposphere moisture is small; more shallow convection and less stratiform precipitation reduce the removal of moisture by precipitation. The factor m₂ γ_q defines a relaxation timescale for moisture anomalies when the $\partial T_2/\partial t$ term in Eq. (28) vanishes. For our normative parameter choices, the relaxation timescale is about a day and half.

With a nozero $\partial T_2/\partial t$ term in Eq. (28), moisture is coupled to T_2 . In this case, a relaxation timescale for moisture alone is not defined, and the $-m_2\gamma_q q$ term acts to reduce the growth rate of the unstable mode. This effect is stronger at lower frequencies, i.e. the moistening effect of J₂ acts to preferentially damp low wavenumbers. More quantitatively, consider small departures in ω from its value for m₂=0, i.e. $\omega=\delta\omega+c_2k+im_1\gamma_qF/b_1$. Plugging this into (29) and ignoring second order terms of $\delta\omega$, we have

$$\delta\omega \approx \frac{m_1 m_2 (F/b_1) \gamma_q^2}{c_2 k + i \left(m_2 + m_1 F/b_1\right) \gamma_q}$$
(30)

Therefore, this damping effect becomes significant for wavenumbers lower than $(m_2 + m_1 F / b_1)\gamma_q / c_2$. With the normative parameter values, this corresponds to a wavelength of 9000km. The effect of m₂ on the growth rate is shown in Figure 10 (thin solid line). With m₂<0, Eq. (28) contains a unstable moisture mode; without the $\partial T_2/\partial t$ term, it has zero phase speed and a growth rate of m₂ γ_q . For general parameter choices, an

effective m₂ $\hat{m}_2 \equiv \frac{b_1 m_2 - b_2 m_1}{b_1 + b_2 \gamma_0}$ should be used and the effective m₂ becomes negative

when $b_1 < 0.6$, $b_2 > 10/3$, $m_1 > 0.5$, or $m_2 < 0.6$, which are unstable regimes in Figure 7 with very small phase speeds. These modes are therefore attributed to a moisture instability described by Eq. (28) with a negative (effective) m_2 . These modes are similar to the standing modes found in KM06 (their Fig. 4a).

Departing from SQE by introducing a finite response time, i.e. replacing Eq. (28) by

$$\frac{\partial q}{\partial t} = -m_1 J_1 - m_2 \gamma_q q$$

$$\frac{\partial J_1}{\partial t} = \tau_J^{-1} \left(-\frac{F}{b_1} \frac{\partial T_2}{\partial t} - J_1 \right)$$
(31)

shifts J₂ out of phase with T₂ and reduces the growth rate. This is similar to the MCD effect discussed in the f=1 case and is stronger for higher wavenumbers. Figure 10 shows the growth rate with the effect of τ_J included (dotted line) and with the effects of both m₂ and τ_J included (diamond symbol). The mathematical reason for the different effects of m₂ and τ_J is simply that the latter involves $\partial/\partial t$ and the former does not.

The above discussion paints the following physical picture for the basic instability in the limiting case II: Start with SQE, zero net moistening from the second mode heating (m₂=0) and no dissipation (ε =0), and with the propagation of a second vertical mode temperature anomaly T₂. The T₂ anomaly modulates deep (or first baroelinic) convective heating J₁ by perturbing the statistical equilibrium between the lower troposphere and the subcloud layer. The result is a J₁ field that lags T₂ by 90° in phase. This changes the moisture field, which lags J₁ by another 90° and is therefore 180° out of phase with T₂. As J₂=- γ_qq , it is in phase with T₂ and causes growth. This basic instability is illustrated schematically in Figure 11 and will be referred to as the moisture-stratiform instability. While an eastward propagating wave is chosen for the illustration, the same instability mechanism also operates in westward propagating or standing waves. In the case of a standing wave, the phase lag will be manifested as a lag in time. Note that while we have used the name "stratiform" following M00, it is intended here to represent both phases of J₂, i.e., both stratiform and shallow/congestus convection. Building upon this basic

instability, we now add the moistening effect of J_2 , which reduces growth rates more strongly at low wavenumbers, and the finite time to approach QE, which reduces growth rates more strongly at high wavenumbers, and the dissipation ε , which damps the waves more or less uniformly in wavenumber. These damping mechanisms shape the otherwise uniform growth rate curve to favor wavelengths of a few thousand kilometers (circles in Figure 10).

3.b.3. Basic difference between the two limiting cases

The following steps shown in Figure 11 are the same in both limiting cases:

(b) \rightarrow (c) \rightarrow (d) \rightarrow (a). The main difference between the two is that in the limiting case II with f=0, the second baroclinic temperature anomaly controls the first baroclinic heating, and the feedback loop illustrated in Figure 11 is complete, giving rise to the moisturestratiform instability, while in the limiting case I with f=1, the first baroclinic temperature anomaly controls the first baroclinic heating, the feedback loop is not complete, and all waves are stable. The basic reason for the different behavior of the two vertical modes is that the first baroclinic heating J₁ is more strongly tied to $\partial T/\partial t$ (controlled by shallow or deep CAPE) while the second baroclinic heating J₂ is more strongly tied to moisture (moisture control). This allows J₂ to be more in phase with T₂ when J₁ is controlled by T₂, but constrains J₁ to be largely in quadrature with T₁ when it is controlled by T₁. While we have taken b₂=0, γ_0 =0 for conceptual simplicity, the same conclusion can be drawn with more general parameter choices, as discussed in Appendix C.

3.b.4. Intermediate cases: 0<f<1

We are unaware of general mathematical results that relate intermediate cases to the two limiting cases in a simple and physically meaningful way. We have therefore examined the model behavior for intermediate values of f empirically. The moisture stratiform instability remains the basic instability (all waves are stable when either m_1 or γ_q is zero), and the moistening effect of J_2 and the MCD effect continue to shape the growth rate curve by reducing the growth rates, more strongly at low and high wavenumbers, respectively. Although, even with $m_2=0$, as f increases, the instability is reduced more strongly at low wavenumbers (Figure 12), indicating the presence of other stabilization effects at low wavenumbers in addition to the moistening effect of J_2 . There is enhanced instability near f~0.2 particularly at higher wavenumbers. This is associated with the resonance effect present in the limiting case I (when $c_2\sim c_1^*$). The larger resonance effects at higher wavenumbers can be understood in mathematical terms. However, given the highly idealized nature of the present model and the strong MCD damping effect at high wavenumbers, the relevance of such resonance to the real atmosphere is not clear.

3.c The case of $\gamma_0 < 0$, $\gamma_q = 0$ and the stratiform instability of Mapes (2000)

As seen in Figure 7d (and Figure 4d), there is a branch of unstable waves with $r_0>1$ (or $\gamma_0<0$) that behaves differently from that with $r_0\leq1$ (or $\gamma_0\geq0$). This represents a case where the background mean convective heating is stronger in the upper troposphere. Its behavior is best exposed by setting $\gamma_q=0$. To simplify the discussion, we will also take $b_2=0$, $\varepsilon=0$, and $\tau_J=0$, although these are not required. The system is now reduced to:

$$\frac{\partial T_1}{\partial t} + c_1 \frac{\partial T_1}{\partial x} = J_{1,eq}$$

$$\frac{\partial T_2}{\partial t} + c_2 \frac{\partial T_2}{\partial x} = \gamma_0 J_{1,eq}$$

$$J_{1,eq} = -f \frac{F}{b_1} \frac{\partial T_1}{\partial t} - (1-f) \frac{F}{b_1} \frac{\partial T_2}{\partial t}$$
(32)

Figure 13a shows that this simple system qualitatively reproduces the $r_0>1$ branch of the unstable modes seen in Figure 7d and Figure 4d. The large growth rates in Figure 13a, particularly those at high wavenumbers, are reduced and come to closer agreement with Figure 7d when an adjustment time to QE ($\tau_J=2hr$) is included (Figure 13b).

The dispersion relation for this system is quadratic and can be readily derived. It is easy to show analytically that a necessary condition for instability is $\gamma_0 < 0$ and that the growth rate is proportional to wavenumber. Therefore, this mechanism depends on positive stratiform heating (negative J₂) being tied to positive deep convective heating (J₁) directly through γ_0 being less than 0 instead of indirectly through J₁'s effect on q. We shall refer to this as the direct stratiform instability mechanism to distinguish it from the moisture-stratiform instability mechanism discussed in section 3.b.

An example of the structure of the unstable waves from Eq. (32) with f=0.5 and γ_0 =-0.2 is shown in Figure 14. With f=0.5, the phase and amplitude relationship between T₁ and T₂ is such that J₁, which is proportional to $\partial(T_1+T_2)/\partial t$, is roughly in opposite phase with T₂. This sets up a feedback loop that is the same as that of M00: when T₂ is negative (cold below and warm above), deep convection is enhanced; with $\gamma_0 < 0$, a negative J₂ (cooling below and heating above) is tied to enhanced deep convection (positive J₁), and amplifies the T₂ anomaly. Therefore, the basic instability mechanism in this regime is

identified to be the same as the stratiform instability of M00. The wave structure is affected by replacing two-way wave equations with one-way wave equations. While not shown, when the two-way wave equations are used with $r_0=1.5$ (i.e. $\gamma_0=-0.2$) and $r_q=0$, the temperature structure of the wave captures the salient features of the observed waves quite well.

The formulation in Eq. (32) is indeed similar to that of M00 and MS01, except that M00 has an additional prognostic equation for the subgrid-scale triggering energy. The effects of T₂ and T₁ on J₁ are similar to their roles in the CAPE calculation in M00 and MS01 except that here J_1 is determined implicitly from $\partial T/\partial t$ based on the QE concept instead of the explicit prognostic approach of M00 and MS01. As discussed in section 2b, the relative importance of $\partial T_2/\partial t$ and $\partial T_1/\partial t$ in determining J₁, as measured by the parameter f, indicates the depth of the troposphere that is in QE regardless of the environmental humidity, and is physically interpreted as the importance of undiluted parcels in the convective mass flux. A similar interpretation can be made for the role of T_2 in the CAPE calculation in MS01 as this includes the effect of entrainment. Values used in MS01 and KM06 imply an f of 0.9. The relative weights of T_1 and T_2 in the CAPE calculation in M00 imply an f value of 0.8, although the role of T₂ on convection is further enhanced by its role in his CIN calculation, which would imply an f value of ~ 0.1 -0.2. The effective f in M00 therefore varies between 0.1 to 0.8, depending on how strong the CIN control is relative to the CAPE control, and can be close to our normative value.

The system of Eq. (32) constrains J_2 to be in opposite phase with J_1 , so there is no tilted heating structure as in observations. The tilt can be introduced with a time lag between J_2 and J_1 :

$$\frac{\partial J_2}{\partial t} = \tau_{J2}^{-1} \left(\gamma_0 J_1 - J_2 \right) \tag{33}$$

as done in M00, where a 3hr time lag is used, representing the time lag between the stratiform phase and the convective phase of a mesoscale convective system (MCS). This, however, provides appreciable tilts only at short wavelengths; a 3hr time lag corresponds to only 270km with a wave speed of 25m/s. For a wavelength of 864km, for example, and a 3hr time lag, J_2 lags $-J_1$ by $\sim 40^{\circ}$ and appreciable tilt is indeed seen in the heating structure. However, for longer wavelengths (for example, the case with a wavelength of 8640km shown in Figure 14), the same time lag produces little tilt (J_2 lags $-J_1$ by $\sim 8^\circ$), as one should expect from Eq. (33). Indications of this behavior are also evident in MS01 (e.g. their Fig.4). Therefore, it is difficult for the basic instability mechanism in this regime ($\gamma_0 < 0$ and $\gamma_q = 0$) to produce the significant tilt seen in the observed heating field of large-scale waves. While we have taken $b_2=0$, $\varepsilon=0$, and $\tau_J=0$ to simplify the discussion, the basic results remain the same without these simplifications. Eq. (33) with an adjustment time of 3hr also has the effect of further reducing the growth rates at high wavenumbers, and selecting waves of synoptic scale (~2000km in wavelength) as the fastest growing (not shown).

As discussed in section 2.b, we have neglected the role of undiluted CAPE on the depth of convection based on the view that all updrafts experience significant entrainment and midtropospheric moisture deficit is the main factor affecting the depth of convection. In this section, as we have set $\gamma_q=0$, one may wish to include the effect of undiluted CAPE and replace Eq. (20) with

$$J_2 = \gamma_0 J_1 - \gamma_T T_2 \tag{34}$$

which changes the second equation in (32) to

$$\frac{\partial T_2}{\partial t} + c_2 \frac{\partial T_2}{\partial x} = \gamma_0 J_{1,eq} - \gamma_T T_2$$
(35)

This adds a simple damping effect on T_2 , which is the same as the cumulus congestus damping effect on the second mode temperature in section 2b3 of M00.

3.d Moisture-stratiform instability versus direct stratiform instability

From the CSRM simulations of K07, which are idealized simulations based on the Tropical Ocean Global Atmosphere Coupled Ocean-Atmosphere Response Experiment (TOGA-COARE) (Webster and Lukas, 1992), there are two pieces of evidence against the direct-stratiform instability being the main instability. First, when vertical advection of moisture is disabled in K07, convectively coupled waves are largely suppressed, while the direct-stratiform instability mechanism is not affected by the removal of vertical moisture advection. Second, substantial tilt in the heating structure is found in K07 across a wide range of wavenumbers. This is also inconsistent with the direct-stratiform instability mechanism. When stratiform heating is tied to deep convective heating with a fixed time lag based on the life cycle of MCSs, the tilt in the heating structure is expected to become increasingly small as wavelength increases. This is noted by Mapes et al. (2006). In contrast, the moisture-stratiform instability requires the vertical advection of moisture and yields substantial tilt in the convective heating structure over a wide range of wavenumbers (Figure 3). Indeed, in its limiting form, Eqs.(27) and (28), $J_2 \text{ lags} - J_1$ by a quarter cycle. The moisture-stratiform instability is therefore more in line with the CSRM simulations of K07, and is suggested as the main instability mechanism in these simulations, and likely in the real atmosphere under TOGA-COARE conditions as well.

Whether and how this might change with the background mean state is a subject of interest and warrants further research.

4. Summary and discussion

In this paper, we have developed a toy model of convectively coupled waves. Its main new feature is a conceptually simple treatment of convection based on the quasiequilibrium concept, simplified for a model of crude vertical structure. For convection in the lower troposphere we neglect the effect of entrainment and for convection reaching the upper troposphere, we emphasize the effect of entrainment and thus the impact of environmental moisture deficit. For realistic model parameters based on the results of CSRM simulations of K07, the toy model produces unstable waves at wavelengths and with structures that compare reasonably well with the CSRM results.

It is of interest to contrast the present treatment with that of M00, which is an influential model of convectively coupled waves. M00 introduced his model by raising the question: "if CIN is in equilibrium with a statistically ubiquitous population of small entraining cumuli, then how can it be a significant factor inhibiting deep-convective cells, which should presumably suffer less entrainment due to their larger size?" This led to his separate treatments for shallow and deep convection, where the role of shallow convection is a simple damping effect on the second mode temperature anomaly, and the effect of inhibition and triggering is emphasized through the effect of convective inhibition (CIN) and subcloud layer kinetic energy (or triggering energy) on the deep convective mass flux. This separate treatment, however, does not resolve the inconsistency raised by M00, and was recognized as a conceptual deficiency by M00, as shallow and deep convection are obviously interrelated. This inconsistency is absent in

our treatment, where CIN is indeed not a significant factor in inhibiting deep-convective cells; instead, mid-troposphere moisture deficit is the main factor. We also eliminate triggering and inhibition from the conceptual picture and consider convection to be in quasi-equilibrium with the large-scale flow. Triggering and inhibition do occur; however, they reflect more of a view on individual storm scale instead of that on a large scale. On a large scale, we maintain that a quasi-equilibrium view is an adequate conceptual simplification.

We further analyzed the basic instability mechanisms of this model. We identified a moisture-stratiform instability, illustrated in Figure 11, which arises from the effect of mid-tropospheric humidity deficit on the depth of convection. We found that the net moistening effect of the second mode convective heating and the finite time to approach QE both act to reduce the growth rates, preferentially at low and high wavenumbers, respectively. These damping mechanisms help to select wavelengths of a few thousand kilometers as the fastest growing. An earlier study (KM06) included moisture in their convective parameterization, but their treatment is conceptually complicated and their analysis did not reveal a clear instability mechanism involving moisture. KM06 concluded that second baroclinic mode low-level moisture convergence plays a major role in the generation of the basic instability, whereas here this effect (included in m₂) is found to damp the waves as discussed in section 3.b.2.

When the background convective heating profile is stronger in the upper troposphere than in the lower troposphere, the model contains an additional instability mechanism. This is named the direct-stratiform instability and is identified to be the same as the stratiform instability of M00. The direct stratiform instability mechanism, however, is inconsistent

with the importance of moisture advection and the substantial tilt in the convective heating structure (especially at low wavenumbers) seen in the CSRM simulations of K07. The moisture-stratiform instability on the other hand is consistent with the CSRM simulation results, and is suggested as the main instability mechanism in these simulations, and likely in the real atmosphere under TOGA-COARE conditions as well. Whether and how this might change with the background mean state is a subject of further research.

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Appendices

A. Parameter Estimation

In this appendix, we try to obtain rough estimates of the parameters used in the simple model. The CSRM simulations of K07 will be used to guide the estimates. In those simulations, a CSRM is coupled to linear gravity wave dynamics and convectively coupled waves spontaneously develop. The reader is referred to K07 for details about the simulations. We will use the first 20 days (i.e. the initial growth period) of the case with a lid at 14km, constant surface fluxes and a wavelength of 10,000km. A longer wavelength (and wave period) is preferable because convection and the large-scale wave can be expected to be closer to statistical equilibrium and the effect of the finite response time of convection, which would complicate the interpretation, is smaller.

We first construct CSRM counterparts of the simple model variables. Vertical mode decomposition (with a lid at 14km) is used to obtain J_1 , J_2 , w_1 , w_2 , T_1 , and T_2 . To be consistent with Eq. (4), the modes are normalized so that their absolute values average to 1. The subcloud layer is defined to be between the surface and 930hPa. The variable q_{mid} is chosen to be that averaged over 400-600hPa. It is important to emphasize that the simple model is a gross simplification of the CSRM simulations (and the real atmosphere). Therefore, viewing the CSRM results in the simple model framework is approximate and uncertainties in the resulting estimates are far greater than those implied by the goodness of the fit. We only intend to use these estimates as educated guesses of plausible values.

With the above cautionary words in mind, we show in Figure 15a the regression of convective moistening (Q_2) of q_{mid} against the two convective heating modes J_1 and J_2 . In the CSRM simulations, the large-scale advective tendencies are explicitly calculated and convective tendencies such as convective moistening and heating are computed as residuals, similar to e.g. Yanai et al. (1973). Contributions from J1 and J2 to convective moistening are shown in red and green, respectively. Their sum reproduces Q₂ almost perfectly on the scale plotted and is omitted. Convective drying (negative Q₂) is dominated by the first heating mode (d_1 =1.3). The second heating mode has a moistening effect (d₂=-1.1). This represents a moistening (drying) effect in the mid-troposphere by congestus (stratiform) convection. Figure 15b shows the regression of the q_{mid} tendency due to vertical advection against w_1 and w_2 , which yields $a_1=1.6$ and $a_2=0.0$. The effect of the second mode is small because the midtroposphere is around the nodal point of w_2 . Similar results are obtained from applying the vertical structures of w_1 and w_2 on the background moisture stratification and integrating from 400-600hPa. The actual time derivative of q_{mid} is the sum of convective drying and vertical moisture advection, and is substantially smaller because these two effects tend to cancel. In particular, there is a large compensation between adiabatic cooling and convective heating associated with the first mode: w_1 is well correlated with J_1 (correlation 0.98) and is only slightly larger (by ~3%) than J_1 . Note that a larger adiabatic cooling (w_1) than convective heating J_1 is consistent with the notion of a positive gross moist stability for the deep convective heating mode (e.g. Emanuel et al., 1994). Combined with the smallness of a₂, it appears reasonable to neglect moisture advection by w₂ and combine convective drying and vertical moisture advection effects of the first mode, as in Eq. (7). This simplified

treatment reproduces the total q_{mid} tendencies reasonably well (Figure 15c). While the estimates are subject to many uncertainties, that $m_1=a_1-d_1$ is positive, i.e. the net effect of deep convective heating, J_1 , is to make the mid-troposphere more humid, is a robust result.

We compute $\partial h_b/\partial t$ as the mass weighted averages of moist static energy tendencies over the depth of the sub-cloud layer. Figure 15d shows a regression of $\partial h_b/\partial t$ by convection against J₁ and J₂ (Eq. (5) with E=0). Contributions from large-scale vertical advection in the subcloud layer are smaller and neglected. This yields b₁=1.0 and b₂=2.3. A positive b₂ implies that convective heating in the lower troposphere is more effective at reducing h_b than that in the upper troposphere on a per unit heating basis. This is perhaps somewhat counter-intuitive, but is quite clear in the CSRM simulations because boundary layer cooling and drying peaks before the maximum first mode heating, i.e. it is shifted towards the congestus phase (Figure 15d). Some indication of this is also seen in the 2day wave study of Haertel and Kiladis (2004).

We now try to constrain the parameters in Eq.(10). This formulation on the control of the height of convection is very approximate, so uncertainties in the estimates are large. To reflect these uncertainties, we simply choose $r_0=1$ and $r_q=0.7$. Figure 15e indicates this is a plausible choice. A better fit can be achieved through a regression, but would convey a false sense of accuracy and is deemed more misleading than informative.

In Figure 15f, we plot the regression of subcloud layer moist static energy to the temperature averaged over the lower troposphere (between 930hPa and 500hPa), assuming that the wave period is sufficiently long so that strict (or close to strict)

statistical equilibrium is satisfied (Eq. (13)). This gives $F\approx4$. This is larger than $\partial s^*/\partial T$ at, say, 3km (~ 285K, ~700hPa), which is ~3. A possible reason for this is that factors such as entrainment may have diluted the h_b variations as air parcels rise through the lower troposphere.

B. Connections between Eq.(3) and Eq.(19)

Let us first add a Newtonian cooling ε in the thermodynamic equations in Eq. (3). Assuming a wave solution of the form exp(i ω t-ikx), and diagonalizing the system, we have:

$$\frac{(i\omega + \varepsilon + ikc_j)(-iw_j + kc_jT_j) = kc_jJ_j}{(i\omega + \varepsilon - ikc_j)(iw_j + kc_jT_j) = kc_jJ_j}$$

$$(36)$$

Eliminating w_i leads to

$$\left(i\omega + \varepsilon - ikc_{j}\right)T_{j} = J_{j}\frac{i\omega + \varepsilon}{i\omega + \varepsilon + ikc_{j}}$$
(37)

For waves with periods substantially shorter than $2\pi/\epsilon$ (~60 days with our choice of ϵ), we have approximately

$$\frac{\partial T_j}{\partial t} + c_j \frac{\partial T_j}{\partial x} = \frac{\omega}{\omega + kc_j} J_j - \varepsilon T_j$$
(38)

Therefore, Eq. (3) is connected to Eq. (19) with

$$J_{j}^{Eq3} = J_{j}^{Eq19} \left(1 + \frac{kc_{j}}{\omega} \right)$$
(39)

Eq. (39) indicates that convective heating is more effective in forcing temperature variations in the one-way wave equations. This is particularly true for the first vertical mode. For waves with a phase speed of 25m/s, the first vertical mode heating is three

times as effective and the second vertical mode heating is twice as effective in the oneway wave equations compared to the two-way wave equations.

C. Limiting cases with general parameter choices

In this appendix, we consider the limiting cases with general parameter choices to extend the results with the simplifying parameter choices presented in Sections 3b and 3c. We shall consider the system to be in SQE. The effect of τ_J is similar to that with the simplifying parameter choices.

When f=1, Eq.(23) becomes

$$J_{1,eq} = \frac{1}{b_1 + b_2 \gamma_0} \left(b_2 \gamma_q q - F \frac{\partial T_1}{\partial t} \right)$$
(40)

We have continued to neglect T_1 's contribution in q^+ . At SQE, we have

$$\frac{\partial T_1}{\partial t} + \hat{c}_1 \frac{\partial T_1}{\partial x} = K_1 \gamma_q q - \hat{\varepsilon}_1 T_1$$

$$\frac{\partial q}{\partial t} = -\hat{m}_1 \frac{F}{b_1} \frac{\partial T_1}{\partial t} - \hat{m}_2 \gamma_q q$$
(41)

where

$$(\hat{\varepsilon}_{1}, \hat{c}_{1}) \equiv (\varepsilon, c_{1}) \frac{b_{1} + b_{2} \gamma_{0}}{F + b_{1} + b_{2} \gamma_{0}} \hat{m}_{1} \equiv \frac{m_{1} + m_{2} \gamma_{0}}{1 + b_{2} \gamma_{0} / b_{1}} \hat{m}_{2} \equiv \frac{b_{1} m_{2} - b_{2} m_{1}}{b_{1} + b_{2} \gamma_{0}} K_{1} \equiv \frac{b_{2}}{F + b_{1} + b_{2} \gamma_{0}}$$

$$(42)$$

Here T_2 is forced by modes of Eq. (41) and does not feed back onto T_1 and q. This is the same as the limiting case I discussed in section 3.b.1 except with the parameters modified and an additional moisture equation.

When f=0, we have

$$J_{1,eq} = \frac{1}{b_1 + b_2 \gamma_0} \left(b_2 \gamma_q q - F \frac{\partial T_2}{\partial t} \right)$$
(43)

Therefore:

$$\frac{\partial T_2}{\partial t} + \hat{c}_2 \frac{\partial T_2}{\partial x} = K_2 \gamma_q q - \hat{\varepsilon}_2 T_2$$

$$\frac{\partial q}{\partial t} = -\hat{m}_1 \frac{F}{b_1} \frac{\partial T_2}{\partial t} - \hat{m}_2 \gamma_q q$$
(44)

where

$$(\hat{\varepsilon}_{2}, \hat{c}_{2}) \equiv (\varepsilon, c_{2}) \frac{b_{1} + b_{2} \gamma_{0}}{b_{1} + (b_{2} + F) \gamma_{0}}$$

$$K_{2} \equiv \frac{-b_{1}}{b_{1} + (b_{2} + F) \gamma_{0}}$$

$$(45)$$

Here T_1 is forced by the modes of Eq. (44), and does not feedback on T_2 and q. This is the same as the limiting case II discussed in section 3.b.2 except with the modified parameters. Comparing Eq. (44) and Eq. (41), we see that the two systems have the same form. In terms of linear stability, the main difference is in the coefficients in front of q in the temperature equation, K_1 and K_2 . Using our normative parameter values and allowing for a reasonable range, K_1 is close to 0.4, and K_2 is close to -1. Therefore, the f=1 case with general parameter choices may be viewed as having a negative effective γ_q .

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Figure Captions

- Figure 1 Phase speed (left) and growth rate (right) as functions of wavenumber from the linearized version of the full model described in section 2c (with 2-way wave equations), using normative parameter values. Modes with positive growth rates are highlighted with circles in the phase speed diagram. The phase speeds are symmetric about 0.
- Figure 2 Physical patterns of the eigenmodes of the linearized full model described in section 2c (with 2-way wave equations) for an eastward propagating wave with a wavelength of 8640km. Normative values are used for all parameters. (a) T1 (solid), T2 (dashed) and q (dotted) as functions of x (zonal distance). (b) J1 (solid) and J2 (dashed) as functions of x. (c) Zonal and height pattern of the combined temperature anomaly. The contour interval is 0.5K. (d) Zonal and height pattern of the combined convective heating anomaly. The contour interval is 2K/day. In both (c) and (d), negative contours are dashed and the zero contour is omitted.
- Figure 3 Phase lag between J1 and -J2 as a function of wavenumber for the linearized full model described in section 2c with normative parameter values.
- Figure 4 Maximum linear growth rates for the linearized full model described in section 2c with individual parameters varied and the other parameters kept at their normative values.

Figure 5 Same as Figure 1 except for the simplified version described in section 3a.

Figure 6 Same as Figure 2 except for the simplified version described in section 3a and a contour interval of 0.5K/day in (d).

Figure 7 Same as Figure 4 but for the system described in section 3a.

Figure 8 Same as Figure 6 except for the limiting case I (f=1) described in section 3.b.1

with b2=0, $\gamma 0$ =0, ϵ =0, τJ =0, m2=0.

- Figure 9 Same as Figure 8, except for limiting case II (f=0) described in section 3.b.2 with b2=0, γ 0=0, ϵ =0, τ J=0, m2=0.
- Figure 10 Growth rates as a function of wavenumber for limiting case II described in section 3.b.2 with m2= $\tau J=\epsilon=0$ (thick solid), $\tau J=\epsilon=0$ (thin solid), m2= $\epsilon=0$ (dotted), and $\epsilon=0$ (diamond symbols), and none of m2, τJ , ϵ is zero (circles). When a parameter is not zero, it takes its normative value.
- Figure 11 A schematic of the moisture-stratiform instability, illustrated for an eastward propagating wave viewed in a reference frame that follows the wave. All fields shown are anomalies. We start with (a) temperature and vertical velocity (arrows) anomalies associated with the wave. The large-scale lifting cools the lower troposphere as part of the wave signal. This induces a positive deep convection anomaly, which cools the subcloud layer to maintain quasi-equilibrium with the large-scale flow (b). The deep convection anomaly also makes the midtroposphere more humid (c). An anomalously moist mid-troposphere allows convection to reach higher, while an anomalously dry one makes convection lower. This produces a convective heating anomaly pattern that is in phase with the original temperature anomaly and causes instability (d).

Figure 12 Growth rates as a function of wavenumber and f with b2=0, γ 0=0, ϵ =0, τ J=0, m2=0.

- Figure 13 (a) Linear growth rate of the unstable mode as a function of wavenumber and r0 for the system described by Eq. (32) and with f=0.5. (b) Same as (a) but with the effect of a 2hr adjustment time to QE included.
- Figure 14 Same as Figure 8, except for the system described by Eq. (32), and with f=0.5 and $\gamma 0$ =-0.2.
- Figure 15 (a) Contributions to convective drying of the mid-troposphere (∂qmid/∂t)conv (black) by -d1J1 (red) and -d2J2 (green) based on a linear regression. (b)
 Contributions to advective moistening of the mid-troposphere (∂qmid/∂t)adv (black) by a1w1 (red) and a2w2 (green) based on a linear regression. (c) Total tendencies of the mid-troposphere humidity ∂qmid/∂t (black) and (a1-d1)J1-d2J2 (red). (d) A linear regression of convective tendencies of boundary moist static energy ∂hb/∂t (black) against J1 and J2. (e) The second mode heating (black) and rq(1.5T1-qmid) (red) with rq=0.7. (f) A linear regression of hb against lower tropospheric temperature Tlow.



Figure 1 Phase speed (left) and growth rate (right) as functions of wavenumber from the linearized version of the full model described in section 2c (with 2-way wave equations), using normative parameter values. Modes with positive growth rates are highlighted with circles in the phase speed diagram. The phase speeds are symmetric about 0.



Figure 2 Physical patterns of the eigenmodes of the linearized full model described in section 2c (with 2-way wave equations) for an eastward propagating wave with a wavelength of 8640km. Normative values are used for all parameters. (a) T_1 (solid), T_2 (dashed) and q (dotted) as functions of x (zonal distance). (b) J_1 (solid) and J_2 (dashed) as functions of x. (c) Zonal and height pattern of the combined temperature anomaly. The contour interval is 0.5K. (d) Zonal and height pattern of the combined convective heating anomaly. The contour interval is 2K/day. In both (c) and (d), negative contours are dashed and the zero contour is omitted.



Figure 3 Phase lag between J_1 and $-J_2$ as a function of wavenumber for the linearized full model described in section 2c with normative parameter values.



Figure 4 Maximum linear growth rates for the linearized full model described in section 2c with individual parameters varied and the other parameters kept at their normative values.



Figure 5 Same as Figure 1 except for the simplified version described in section 3a.



Figure 6 Same as Figure 2 except for the simplified version described in section 3a and a contour interval of 0.5K/day in (d).



Figure 7 Same as Figure 4 but for the system described in section 3a.



Figure 8 Same as Figure 6 except for the limiting case I (f=1) described in section 3.b.1 with $b_2=0$, $\gamma_0=0$, $\epsilon=0$, $\tau_J=0$, $m_2=0$.



Figure 9 Same as Figure 8, except for limiting case II (f=0) described in section 3.b.2 with $b_2=0$, $\gamma_0=0$, $\epsilon=0$, $\tau_J=0$, $m_2=0$.



Figure 10 Growth rates as a function of wavenumber for limiting case II described in section 3.b.2 with $m_2=\tau_J=\epsilon=0$ (thick solid), $\tau_J=\epsilon=0$ (thin solid), $m_2=\epsilon=0$ (dotted), and $\epsilon=0$ (diamond symbols), and none of m_2 , τ_J , ϵ is zero (circles). When a parameter is not zero, it takes its normative value.



Figure 11 A schematic of the moisture-stratiform instability, illustrated for an eastward propagating wave viewed in a reference frame that follows the wave. All fields shown are anomalies. We start with (a) temperature and vertical velocity (arrows) anomalies associated with the wave. The large-scale lifting cools the lower troposphere as part of the wave signal. This induces a positive deep convection anomaly, which cools the subcloud layer to maintain quasi-equilibrium with the large-scale flow (b). The deep convection anomaly also makes the midtroposphere more humid (c). An anomalously moist mid-troposphere allows convection to reach higher, while an anomalously dry one makes convection lower. This produces a convective heating anomaly pattern that is in phase with the original temperature anomaly and causes instability (d).



Figure 12 Growth rates as a function of wavenumber and f with b₂=0, γ_0 =0, ϵ =0, τ_J =0, m_2 =0.



Figure 13 (a) Linear growth rate of the unstable mode as a function of wavenumber and r_0 for the system described by Eq. (32) and with f=0.5. (b) Same as (a) but with the effect of a 2hr adjustment time to QE included.



Figure 14 Same as Figure 8, except for the system described by Eq. (32), and with f=0.5 and γ_0 =-0.2.



Figure 15 (a) Contributions to convective drying of the mid-troposphere $(\partial q_{mid}/\partial t)_{conv}$ (black) by $-d_1J_1$ (red) and $-d_2J_2$ (green) based on a linear regression. (b) Contributions to advective moistening of the mid-troposphere $(\partial q_{mid}/\partial t)_{adv}$ (black) by a_1w_1 (red) and a_2w_2 (green) based on a linear regression. (c) Total tendencies of the mid-troposphere humidity $\partial q_{mid}/\partial t$ (black) and $(a_1-d_1)J_1-d_2J_2$ (red). (d) A linear regression of convective tendencies of boundary moist static energy $\partial h_b/\partial t$ (black) against J_1 and J_2 . (e) The second mode heating (black) and $r_q(1.5T_1-q_{mid})$ (red) with $r_q=0.7$. (f) A linear regression of h_b against lower tropospheric temperature T_{low} .

Tables:

Table 1 A summary of parameters used in the simple model

Symbol	Normative values	Unit	Description
b1,b2	1, 2		Reduction in h_b per unit J_1 and J_2 (Eq.(5))
a ₁ ,a ₂	1.4, 0	_	Increase in q_{mid} (by advection) per unit w_1 and w_2 , Eq. (6)
d_1, d_2	1.1, -1	_	Decrease in q_{mid} per unit J_1 and J_2 , Eq. (6)
m ₁ ,m ₂	0.3, 1	_	Increase in q_{mid} per unit J ₁ and J ₂ , Eq. (7), $m_{1,2}=a_{1,2}-d_{1,2}$
r ₀	1	_	Background mean U/L ratio, Eq.(10)
γο	0		$(1-r_0)/(1+r_0)$
r _q	0.7	1/day	Dependence of the U/L ratio on moisture deficit, Eq.(10)
$\gamma_{ m q}$	0.7	1/day	$2r_{q}/(1+r_{0})$
F	4	—	Ratio between saturation moist static energy and temperature, Eq. (14)
f	0.5	_	Relative weight used to linearly combine T_1 and T_2 , Eq. (14)
$ au_{ m L}$	1/12	day	Adjustment time to approach QE over the lower troposphere
c ₁ ,c ₂	1, 0.5	50m/s	Dry speeds of the first and second mode
3	1/10	1/day	Damping coefficient