



The capacity of the human iliotibial band to store elastic energy during running

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22 Abstract

23 The human iliotibial band (ITB) is a poorly understood fascial structure that may contribute to energy savings during locomotion. This study evaluated the capacity of the 24 25 ITB to store and release elastic energy during running, at speeds ranging from 2-5 m/s, 26 using a model that characterizes the three-dimensional musculoskeletal geometry of the 27 human lower limb and the force-length properties of the ITB, tensor fascia lata (TFL), and gluteus maximus (GMax). The model was based on detailed analyses of muscle 28 architecture, dissections of 3-D anatomy, and measurements of the muscles' moment 29 30 arms about the hip and knee in five cadaveric specimens. The model was used, in 31 combination with measured joint kinematics and published EMG recordings, to estimate 32 the forces and corresponding strains in the ITB during running. We found that forces 33 generated by TFL and GMax during running stretch the ITB substantially, resulting in 34 energy storage. Anterior and posterior regions of the ITB muscle-tendon units (MTUs) show distinct length change patterns, in part due to different moment arms at the hip 35 36 and knee. The posterior ITB MTU likely stores more energy than the anterior ITB MTU 37 because it transmits larger muscle forces. We estimate that the ITB stores about 1 J of 38 energy per stride during slow running and 7 J during fast running, which represents 39 approximately 14% of the energy stored in the Achilles tendon at a comparable speed. 40 This previously unrecognized mechanism for storing elastic energy may be an 41 adaptation to increase human locomotor economy.

42

43 Introduction

44 Because bipedalism is a fundamental derived feature of hominins (species more closely related to humans than chimpanzees), many distinctive features of the human 45 46 spine and lower extremity are adaptations to improve bipedal locomotor performance. 47 Many adaptations for standing and walking, for example, appear early in hominin 48 evolution including a inferiorly-oriented foramen magnum, a lordotic lumbar spine, and a 49 sagittally-oriented ilium (see Aiello and Dean, 1990; Zollikofer et al., 2005). Additional 50 features that first appear later in the genus Homo may reflect selection for endurance 51 running, including a stabilized sacroiliac joint, an expanded attachment of gluteus 52 maximus, and shorter toes (Bramble and Lieberman, 2004; Lieberman et al., 2006; 53 Rolian et al., 2009). Although the selective factors underlying the evolution of both 54 walking and running are debated, it is likely that locomotor economy played a key role. Hypothesized energy-saving features for walking include long legs and dorsally oriented 55 56 ischia (Crompton et al., 1998; Pontzer et al., 2009; Robinson, 1972; Sockol et al., 2007). 57 Energy saving features for running in the genus *Homo* include a long, compliant Achilles 58 tendon and a spring-like median longitudinal arch, which are known to store and recover 59 elastic energy during running in other vertebrates (Biewener, 2003; Ker et al., 1987; Roberts, 2002). In addition, the human lower extremity has a number of fascial 60 structures with elastic properties that are not present in apes, but whether these 61 62 structures store energy or serve another function remains poorly understood. One of the most interesting of these structures is the iliotibial band (ITB). The ITB 63

64 is a thickening of the lateral fascia of the thigh that originates on the pelvis and inserts
65 on the tibia; it receives muscle fibers from the tensor fascia lata (TFL) anteriorly and

66 from the gluteus maximus (GMax) posteriorly (Gottschalk et al., 1989; Gray et al., 1995; Kaplan, 1958; Ober, 1936; Stern, 1972). The ITB is traditionally considered to function 67 as a "strut" during walking, stabilizing the hip in the frontal plane (Gottschalk et al., 68 69 1989; Inman, 1947; Kaplan, 1958). However, the high compliance of the ITB (Butler et 70 al., 1984; Derwin et al., 2008; Gratz, 1931), the fact that it crosses both the hip and 71 knee, and the presence of in-series muscles suggest that the ITB may play other roles. 72 If the ITB stretches substantially while transmitting muscle forces, storing elastic energy, 73 then it may decrease the metabolic cost of locomotion. Prior studies have estimated that 74 energy recovered from the Achilles tendon during running reduces muscle work by as 75 much as 35% (Alexander and Bennet-Clark, 1977; Ker et al., 1987). Whether the ITB 76 also stores and recovers elastic energy, and how this compares to Achilles tendon 77 energy recovery, is unknown.

As a first step toward evaluating the ITB's role in locomotor economy, this study 78 79 examined the capacity of the ITB to store elastic energy at running speeds ranging from 80 2 to 5 m/s. We hypothesized that forces generated by TFL and GMax stretch the ITB 81 during running, storing elastic energy that may be recovered later in the stride. We 82 tested this hypothesis by developing a musculoskeletal model of the ITB and inserting 83 muscles. Our model characterizes the 3-D skeletal geometry, the hip and knee 84 kinematics, and the attachments and force-length (F-L) properties of the ITB, TFL and 85 GMax for an average-sized adult male (femur length: 39.8 cm; tibia length: 36.2 cm). Because existing representations of TFL and GMax were not sufficiently accurate for 86 87 this study, we performed detailed analyses of these muscles' architecture and 88 measured their moment arms (MAs) about the hip and knee in cadaveric specimens.

The TFL has largely been neglected in previous studies of muscle architecture (e.g., 89 90 Ward et al., 2009; Wickiewicz et al., 1983) and locomotor function (e.g., Dorn et al., 91 2012: Sasaki and Neptune, 2006), despite being active during running (Andersson et 92 al., 1997; Mann et al., 1986; Montgomery et al., 1994; Paré et al., 1981). GMax is 93 routinely modeled as a uniarticular hip extensor that inserts on the femur (e.g., Arnold et 94 al., 2010; Delp et al., 1990), despite evidence that a substantial portion of GMax inserts 95 on the ITB (Gray et al., 1995; Stern, 1972). Our refined musculoskeletal model, which addresses these limitations, is available on SimTK (simtk.org). Using this model, we 96 97 estimated the forces transmitted to anterior and posterior regions of the ITB at body 98 positions corresponding to running, predicted the length changes of each region, and 99 calculated the corresponding ITB strain energies over the course of a stride based on 100 published measurements of the tissue's elastic modulus (Butler et al., 1984; Derwin et 101 al., 2008).

102

103 Materials and methods

104 Muscle architecture measurements

We characterized the isometric force-generating capacity of TFL and GMax based on measurements of muscle architecture in three formalin-fixed human cadavers (Table 1). Specimens were dissected and the muscles isolated and removed. Total mass (*M*) of each muscle was measured; in addition, the masses of four regions of the GMax were measured separately. A muscle fascicle was carefully dissected from each region of GMax and from two regions of TFL and the fascicle lengths (L_f) measured. Surface pennation angles between the fascicles and ITB were also measured. Under

magnification, muscle fiber bundles were isolated from each fascicle and mounted on slides. Following Lieber et al. (1990), bundle sarcomere length (L_s) was determined by laser diffraction and used to calculate optimal fascicle length (L_t):

115
$$L_f = L_f' \left(\frac{2.7 \mu m}{L_s'} \right) \tag{1}$$

where 2.7 µm is the optimal sarcomere length for human muscle (Lieber et al., 1994).
Physiological cross-sectional area (*PCSA*) was calculated from muscle mass and
optimal fascicle length (Powell et al., 1984):

119
$$PCSA = \frac{M}{\rho \cdot L_f}$$
(2)

where ρ is muscle density (1.056 g/cm³; Mendez and Keyes, 1960). Our architecture data for GMax are consistent with data reported by Ward et al. (2009).

122 Muscle moment arm measurements

123 We measured MAs of the muscle-ITB paths in five fresh frozen cadaveric hemi-124 pelvises obtained from MedCure (Portland, OR). MAs were determined for hip 125 flex/extension, rotation, ab/adduction, and knee flex/extension using the tendon 126 excursion method (An et al., 1984; Brand et al., 1975). We approximated TFL with two 127 Kevlar thread paths (Figure 1A&B) and GMax with four paths (Figure 1A&C). The ITB 128 was left intact during these measurements. Each thread was anchored to a screw eye 129 at the path's insertion, routed over the ITB through plastic tubing to a screw eye at the 130 path's origin, and attached to one of two cable-extension position transducers (PTX101, 131 Celesco, Canoga Park, CA) that measured length changes with an accuracy of ± 0.32 132 mm while applying a tension of 1.4 or 2.8 N. The tubing ensured a repeatable path

along the surface of the ITB and decreased friction. Detailed procedures for definingeach path are described in supplementary materials.

135 Hip and knee angles were measured simultaneously with muscle-ITB length 136 changes using a motion tracking system (Polhemus Fastrak, Colchester, VT) and 137 custom software (LabView, National Instruments Corporation, Austin, TX). Receivers 138 were rigidly attached to the pelvis, femur, and tibia to track the segments' positions and 139 orientations. Segment coordinate systems were defined along anatomical axes by 140 digitizing bony landmarks and determining the hip center (Figure S1), as described in 141 the supplementary materials. For each muscle-ITB path, we digitized the origin, 142 insertion and key "via" points that constrained the path with hip or knee motion. We also 143 tracked the relative motions of nine marker pairs sutured along the ITB using high-144 speed video. These data guided development of the model and were analyzed to 145 determine the hip and knee angles at which the anterior and posterior ITB began to 146 stretch.

147 Each specimen was mounted in a custom frame (Figure 2) that allowed 148 independent control of hip flex/extension, rotation, ab/adduction, and knee flexion 149 following Arnold et al. (2000). Alignment and mounting of the specimen comprised four 150 main steps, each performed with real-time feedback to ensure that the pelvis, femur, 151 and tibia were secured to within 5 mm and 2° of the desired alignment. First, the pelvis 152 was secured to a table and aligned with either its medial-lateral axis (for flex/extension 153 MAs) or anterior-posterior axis (for ab/adduction MAs) perpendicular to the table. 154 Second, the femur was mounted on a cart equipped with two concentric rings. The 155 femur was secured to the inner ring so that the femur's long axis (from hip center to the

156 midpoint between femoral epicondyles) was centered perpendicular to the plane of the 157 rings. Third, the base of the cart was adjusted so that its wheels rolled in an arc about 158 the specimen's hip center. Fourth, the tibia was secured to a locking hinge attached to 159 the inner ring. When measuring knee MAs, the hinge was removed and the tibia was 160 flexed and extended. When measuring hip rotation MAs, the inner ring was rotated 161 relative to the outer ring, which internally and externally rotated the hip. When 162 measuring hip flex/extension or ab/adduction MAs, the cart was rotated about the 163 specimen's hip center, thereby flex/extending or ab/adducting the hip. When measuring 164 MAs about one axis, the other axes were locked in a neutral position (hip flexion = 0° , hip rotation = 5° , hip adduction = 0° , knee flexion = 0°). To verify alignment, we 165 166 monitored coupling of hip angles and ensured that hip adduction varied $< 2^{\circ}$ and hip 167 rotation $< 4^{\circ}$ over a 75° range of flexion. When the specimen was aligned for hip ab/adduction, we ensured that hip flexion varied $< 2^{\circ}$ and hip rotation $< 4^{\circ}$ over a 50° 168 169 range of ab/adduction.

To measure muscle-ITB MAs, the excursion of each thread path was recorded while slowly moving the specimen through its ranges of hip and knee motion. Excursion and joint angle data were sampled at 10 Hz (National Instruments BNC-2090 A/D converter). The lengthening excursion versus joint angle data were fit with a fourth order polynomial, and the derivative of the polynomial was averaged across trials to estimate the MA. A minimum of five trials was collected for each condition.

Following MA measurements, muscles were freed, cleaned of fat and connective
tissue, and weighed (Table 2). In two specimens, the regions of GMax were carefully

dissected to determine the relative masses of the portions that insert on the ITB versusthe femur.

180 Model of TFL, Gmax, and ITB F-L properties

181 We modified the paths of TFL and GMax muscle-tendon units (MTUs) in the 182 model reported by Arnold et al. (2010) to match our digitized attachments and MA data 183 (Figure 3). Using SIMM (Software for Interactive Musculoskeletal Modeling, v7.0, 184 MusculoGraphics, Santa Rosa, CA), we initially created two paths for TFL and eight for 185 GMax (four to the ITB and four to the femur). Via points and wrapping surfaces were 186 iteratively adjusted so that the model's paths reproduced the three-dimensional paths 187 digitized during the experiments and the model's MAs matched the experimentally 188 determined MAs. Because the model's MAs are extremely consistent with our 189 experimental data (Figures 4 & S2), we are confident that the model accurately predicts 190 length changes of these MTUs.

191 To estimate strain in regions of the ITB during running, we created three 192 additional MTUs, representative of the major paths of ITB force transmission 193 determined from our experiments (Figure 3B,C). One path accounts for force 194 transmitted by the anterior ITB when TFL is active (TFL-ITB_{ant}). The other paths account 195 for the cumulative force transmitted by the posterior ITB when superior (GMax1,2-196 ITB_{post1}) or inferior (GMax3,4-ITB_{post2}) portions of GMax are active. Attachments and via 197 points of each path were iteratively adjusted to yield average MAs of the combined 198 MTUs (Figures 4). This model represents the muscles as independent, proximal-to-199 distal MTUs, even though the ITB is multi-layered and loaded from different directions, 200 based on detailed dissections and on biaxial testing of goat fascia lata, which showed

that the fascia's material properties are not strongly influenced by its biaxial strain
environment (Eng et al., 2014).

203 We used a Hill-type muscle model (Delp et al., 1990; Zajac, 1989) to estimate 204 isometric forces generated by TFL-ITB_{ant}, GMax1,2-ITB_{post1}, and GMax3,4-ITB_{post2} at 205 different activation levels. Two parameters, maximum isometric force (F_{max}) and optimal 206 fiber length (L_{opt}), scaled normalized active and passive F-L curves to each muscle 207 (Table S1). F_{max} and an additional parameter, tendon slack length (L_{TS}), scaled a normalized "tendon" F-L curve to each MTU. We specified parameters for each MTU 208 209 based on our architecture measurements and data reported by Ward et al. (2009). We 210 adjusted L_{TS} such that ITB_{ant} and ITB_{post} began to stretch passively at hip and knee 211 angles consistent with our experimental data.

For each MTU, we created a normalized F-L curve for the ITB (Figure 5) based on published material properties of the human ITB (Butler et al., 1984; Derwin et al., 2008). We assumed a transition strain of 4% based on data from goat fascia lata (Eng et al., 2014). Above 4% strain, we assumed a linear relationship between force and strain with a normalized stiffness (\tilde{k}) determined using the ITB's elastic modulus (*E*), the muscle's *F*_{max}, and the ITB's effective cross-sectional area (*a*):

218
$$\tilde{k} = \frac{E \times a}{F_{\max}}$$

The effective cross-sectional area of the ITB was calculated from measurements of thickness and width in cadaveric specimens (see Table S2). The width of each ITB region was measured while placing tension on the inserting muscle and visually assessing ITB strain. We used an elastic modulus of 400 MPa, which is consistent with values reported in the literature (Butler et al., 1984; Derwin et al., 2008; Hammer et al.,

2012; Steinke et al., 2012). Below 4% strain, in the toe region, we decreased stiffness by a factor of 2/3. At F_{max} , the ITB strains 5-11% in our model, which seems plausible given the range of yield strains reported in the literature (10-27%; (Butler et al., 1984; Hammer et al., 2012; Hinton et al., 1992). The regional variation in strain at F_{max} is consistent with our measurements of ITB thickness, which are relatively uniform in anterior and posterior regions despite the fact that the inserting muscles differ substantially in force-generating capacity.

231 Assessment of ITB energy storage

232 We used our model in combination with published joint kinematics and EMG 233 recordings to examine the capacity of the ITB to store elastic energy during running. 234 First, we calculated the lengths of the MTUs at hip and knee angles corresponding to 235 running using data from 10 experienced runners, at speeds of 2, 3, 4, and 5 m/s 236 (Hamner and Delp, 2013). Next, we divided MTU lengths into muscle fiber lengths and 237 ITB lengths by independently activating each MTU in the model and solving for the 238 lengths at which the muscle and ITB forces were equivalent, accounting for pennation 239 angle. Maximum activation levels for running were assumed to range between 20% and 240 65% of the EMG activation measured during a maximum voluntary contraction (MVC). 241 In particular, we set each muscle's maximum activation to 20%, 35%, 50%, or 65% to 242 estimate ITB strains during running at 2, 3, 4, and 5 m/s, respectively. These values are 243 based on reported maximum activations of 20% MVC in GMax and TFL during level 244 walking (Perry, 1992), 40% MVC in GMax and TFL during level running at 4.0 m/s (Montgomery et al., 1994), and 65% MVC in GMax during level running at 4.5 m/s 245 246 (Swanson and Caldwell, 2000). Time-varying patterns of activity were derived from

247 EMG recordings reported for GMax and TFL (Jönhagen et al., 1996; Montgomery et al., 248 1994; Paré et al., 1981; Swanson and Caldwell, 2000), which we scaled to the 249 maximum activation at each speed (Figure 7). Lastly, we estimated energy storage 250 capacity at each speed by integrating the ITB F-L curves from L_{TS} to peak ITB length 251 during running. Length changes of the ITB were determined relative to slack length. 252 Total elastic energy stored in the posterior ITB was calculated as the sum of the 253 energies stored in GMax1,2-ITB_{post1} and GMax3,4-ITB_{post2}. We assessed the sensitivity 254 of our analysis to the F-L properties by varying normalized stiffness by ±20% and 255 transition strain by $\pm 2\%$ (Figure 5) and re-calculating energy storage.

256

257 Results

258 The TFL and GMax MTUs in our model undergo substantial excursions during 259 running (Figure 6). Because of its hip flexion and knee extension MAs, TFL-ITB_{ant} is 260 maximally stretched during early swing, when the hip is extended and the knee flexed 261 (Figure 3C). EMG recordings show that TFL is highly activated during this time (Figures 262 6 & 7) (Montgomery et al., 1994; Paré et al., 1981). In contrast, because of their role in 263 hip extension and knee flexion MAs, GMax-ITB_{post1} and GMax-ITB_{post2} are maximally 264 stretched during late swing, when the hip flexes and the knee extends (Figure 3C). 265 EMG recordings show that GMax is highly activated during this time (Figures 6 & 7) 266 (Jönhagen et al., 1996; Swanson and Caldwell, 2000). Inferior portions of GMax 267 lengthen about 7% more than proximal portions, due to larger hip extension MAs when 268 the hip is flexed.

269 The largest strains in ITB_{ant} occur in early swing (Figure 7A), with ITB_{ant} stretching 270 0.9 to 1.7 cm beyond slack length in our model. TFL muscle fiber length is longer than 271 optimal when it begins generating force in late stance, and near optimal when it is 272 maximally activated in early swing. Peak strains in ITB_{post} occur in late swing (Figure 273 7B), with ITB_{post} stretching 1.4 to 3.0 cm beyond slack length in our model. GMax3,4 is 274 shorter than optimal length when it begins generating force in mid swing; however, it is 275 stretched beyond optimal length as the hip flexes in swing. In late swing, when GMax3,4 276 is maximally activated, it operates near optimal length and generates forces that stretch 277 ITB_{post} in our model. A similar pattern occurs in GMax1,2-ITB_{post2}. Passive strains in the 278 ITB, without muscle activation, are relatively small in our model. ITB_{ant} strains 1.7% and 279 ITB_{post} strains 1.1% over the stride cycle when the muscles are not activated.

280 Because the TFL and GMax MTUs are stretched to relatively long lengths when 281 the muscles are active during running, both anterior and posterior regions of the ITB in 282 our model have the capacity to store elastic energy. We estimate that ITB_{ant} strains 283 about 4% during running at 5 m/s, which means that the ITB_{ant} may store nearly 1 J of energy per stride during early swing (Figure 8A). ITB_{post1} and ITB_{post2} strain about 4% 284 285 during slow running and 7% during faster running in late swing when GMax is maximally 286 active in our model. These data suggest that the ITB_{post} may store as much as 6 J per 287 stride during late swing (Figure 8B).

288

289 **Discussion**

290 This is the first study to quantitatively characterize the 3-D musculoskeletal 291 geometry of the human ITB and its inserting muscles. Dissections confirmed that all

fibers of TFL insert into the anterior ITB and a large fraction of GMax (40-70% by mass)
inserts into the posterior ITB. Thus, the ITB likely transmits substantial force.

Additionally, our MA measurements confirmed that the inserting muscles have relatively large MAs about the hip, and thus undergo large MTU excursions, with hip flexion and extension. In combination, the ITB's high compliance and its potential to transmit force while changing length, suggest a plausible, previously unrecognized mechanism for storing elastic energy during running.

We created a model that characterizes the geometry and F-L properties of the ITB, TFL, and GMax to test the hypothesis that forces generated by TFL and GMax stretch the ITB during running, storing elastic energy. Analysis of the model revealed that the ITB has the capacity to store 7 J per stride during running at 5 m/s. The posterior ITB stores substantially more energy than the anterior ITB because it transmits larger muscle forces.

How does the amount of energy stored in the ITB during running compare to energy stored in the Achilles tendon? Using a 3-D model and static optimization, Lai et al. (2014) estimated that the soleus and gastrocnemius store 40-50 J per stride in the Achilles tendon at slow to fast running speeds (3.5 – 5 m/s), an estimate consistent with previous experimental studies (Alexander and Bennet-Clark, 1977; Hof et al., 2002; Ker et al., 1987). We therefore calculate that the combined anterior and posterior ITB stores 14% as much energy as the Achilles tendon at a 5 m/s pace.

To provide additional context, we compared energy stored in the ITB to hip muscle work during running. Sasaki and Neptune (2006) used a muscle-driven dynamic simulation to estimate the mechanical work performed by hip muscles and series elastic

elements during running at 2.4 m/s. They reported that the hip extensors do 40 J of
work per stride during stance, while the hip flexors do 6 J of work during swing.
Recovery of 2 J from ITB_{post} during slow running could account for 5% of the work done
by hip extensors in stance, while recovery of 0.3 J from ITB_{ant} could contribute 5% of the
work done by hip flexors in swing. Although the extent to which energy recovery would
drive selection for endurance running is unknown, these comparisons suggest that
energy storage in the ITB is not negligible.

322 This analysis has several limitations. First, although our data confirm that forces 323 generated by TFL and GMax stretch the ITB during running, storing useful energy, our 324 study did not test whether the human ITB reduces muscle work or enhances locomotor 325 economy. Second, uncertainty exists in the parameters used to derive the F-L curves. 326 For example, our measures of ITB width and thickness in cadaveric specimens may not 327 be representative of healthy young subjects, thus potentially underestimating ITB 328 stiffness. However, varying normalized stiffness by $\pm 20\%$ and transition strain by $\pm 2\%$ 329 altered our estimates of energy storage by only 0.1 J in the anterior ITB and by 1.2 J in 330 the posterior ITB at the fastest running speed. At the slowest running speed, varying 331 stiffness and transition strain altered our estimates of energy storage by about 0.05 J. 332 Thus, we are reasonably confident in our model of the ITB's force-strain behavior and 333 that the ITB contributes to energy storage at all running speeds. Third, we estimated the 334 peak forces generated by TFL and GMax ignoring the muscles' force-velocity (F-V) 335 properties and assuming the muscles' activation patterns during running. If the muscles 336 shorten substantially during running, or if we overestimated activation, then we likely 337 overestimated ITB energy storage. It is plausible, however, that the ITB's length and

compliance allow GMax to operate nearly isometrically when generating maximum force
in late stance, mitigating the effects of F-V properties on muscle-ITB mechanics. In the
running simulations described by Lai et al. (2014), muscles inserting on the Achilles
tendon contracted nearly isometrically across a range of running speeds. Lastly, we
estimated the capacity of the ITB to store elastic energy during running but not walking.
It is likely that the ITB transmits smaller forces, and thus stores less energy, during
walking than reported here.

345 Our study has implications for understanding the evolution of human bipedalism. 346 While these data do not exclude the possibility that the ITB stores substantial energy 347 during walking, selection for the capacity to run long distances would have presented 348 unique demands on the anatomy and physiology of Homo (see Bramble and Lieberman 349 (2004) for review). Among these demands is the need to efficiently accelerate the swing 350 limb, which is long and massive in humans (14% body mass) compared to chimpanzees 351 (9% body mass; Zihlman and Brunker, 1979). The human ITB is stretched substantially 352 just before swing, when the TFL is active and the hip is extending (Figures 6 & 7). 353 Subsequent recoil of the ITB may help accelerate the swing limb. Although the 354 energetic cost of running is primarily determined by muscle forces that support the body 355 during stance (Kram and Taylor, 1990), the cost of accelerating the swing limb may be 356 as much as 27% of total metabolic cost (Marsh et al., 2004; Modica and Kram, 2005; 357 Myers and Steudel, 1985). Thus, selection for increased running economy may have 358 favored traits that increase swing phase energy recovery in *Homo*. The need to 359 decrease locomotor costs may also help explain the expansion of GMax evident in 360 *Homo*. This adaptation is thought to play a role in trunk stabilization during endurance

361 running (Lieberman et al., 2006), but it may also facilitate elastic energy storage by 362 increasing the forces transmitted to the ITB as it is stretched in late swing.

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377

376

379 Figure legends

380

Figure 1. A: Lateral view of the human ITB showing paths of the inserting muscles, TFL
 and GMax, as characterized during the moment arm measurements. B: Lateral diagram
 showing the anterior and posterior paths of TFL. C: Posterior diagram showing the
 superior (Gmax1,2) and inferior (GMax3,4) regions of GMax. Muscle-ITB paths are
 described in the supplementary materials.

386

387 Figure 2. Hardware and procedure for measuring hip ab/adduction and rotation moment 388 arms. The hardware consisted of a fixed table for aligning and securing the pelvis, an 389 adjustable cart for moving the femur through a range of hip ab/adduction angles, and a 390 set of concentric rings for rotating the femur about its mechanical axis, following Arnold 391 et al. (2000). Receivers (shown in gray) were rigidly attached to the pelvis, femur, and 392 tibia to track their motions in real time. 1: The pelvis was secured to a fixed table with its 393 anterior-posterior axis perpendicular to the table. 2: The femur was secured to the inner 394 of the two rings so that the femur's long axis was centered perpendicular to the plane of 395 the rings. 3: The bases of the cart were adjusted so that the cart's wheels rolled in an 396 arc about the specimen's hip joint center. 4: The tibia was secured to a locking hinge. 397 Hip flex/extension moment arms were measured by re-orienting the pelvis on the table 398 so that its medial-lateral axis was perpendicular to the table. More details are provided 399 in the supplementary materials.

400

401 Figure 3. Lower extremity model modified from Arnold et al. (2010). A: Lateral view 402 showing the two TFL-ITB paths that reproduce our experimental data. B: Posterior view 403 showing the four GMax-ITB paths originating on the ilium, sacrum, and coccyx and 404 inserting on the ITB. C: Lateral view of the combined MTU paths used to estimate energy storage. TFL-ITB_{ant}, GMax1,2-ITB_{post1}, and GMax3,4-ITB_{post2} paths are shown at 405 406 touchdown, midstance, toeoff, and midswing during running at 5 m/s. The TFL-ITBant 407 MTU is maximally stretched in early swing, while the GMax-ITB_{post} MTUs are most 408 stretched during late swing.

409

410 Figure 4. Hip and knee moment arms of TFL-ITB_{ant} and GMax-ITB_{post} compared with 411 experimental data. A: TFL has a large hip flexion MA that increases as the hip flexes. B: 412 TFL has a large hip abduction MA that increases with hip abduction. C: The most 413 posterior part of TFL has a small knee extension MA that decreases with knee flexion. 414 D.G: All portions of GMax that insert on the ITB have large hip extension MAs. E: The 415 superior portions of GMax have hip abduction MAs. H: The inferior portions of GMax 416 have hip adduction MAs. F.I: The portions of GMax that insert on the ITB have small 417 knee flexion MAs. Solid lines and shaded regions indicate the means and standard 418 deviations of experimentally determined MAs from five cadaveric limbs. A-C: Dashed 419 lines show the MAs of TFL1-ITB (dark gray), TFL2-ITB (light gray), and the combined 420 TFL1,2-ITB_{ant} (black) predicted by our model. D-I: Dashed lines show the MAs (from 421 superior to inferior) of GMax1 (dark gray), GMax2 (light gray), GMax3 (dark gray), 422 GMax4 (light gray), and the combined paths for GMax1,2-ITBpost1 (black, D-F) and 423 GMax3,4-ITB_{post2} (black, G-I) as predicted by our model. Note the y-axes have different 424 scales.

- 425
- 426 **Figure 5.** Normalized force-length curves for anterior and posterior regions of the ITB
- 427 derived from experimental data (Butler et al., 1984; Derwin et al., 2008; Eng et al.,
- 428 2014). Curves are shown for TFL-ITB_{ant} (short dash), GMax1,2-ITB_{post1} (long dash), and
- 429 GMax3,4-ITB_{post2} (dot-dash) with shaded regions indicating $\pm 20\%$ stiffness used in the
- 430 sensitivity analysis. The ITB is more compliant than tendon (solid line), as shown by the
- typical tendon force-length curve generated by Millard et al. (2013) and by ultrasound based measures of tendon force-length properties reported by Magnusson et al. (2001;
- 432 light gray). This figure is adapted from figure 3 in Millard et al. (2013).
- 434
- Figure 6. Length changes of TFL-ITB and GMax-ITB MTUs during fast running (5 m/s).
 TFL-ITB_{ant} (light gray) stretches during stance phase, while GMax1,2-ITB_{post1} (dark
 gray) and GMax3,4-ITB_{post2} (black) stretch during the swing phase. Regions of
 intermediate muscle activity (10-30% activation; intermediately thickened portion of
 each curve) and maximal muscle activity (31-65% activation; thickened portion of each
 curve) demonstrate that these muscles are maximally active when the MTU is near
- 441 maximum length.
- 442
- 443 Figure 7. TFL-ITB_{ant} and GMax3,4-ITB_{post} activation patterns over the stride cycle. For 444 each muscle, the time-varying pattern was scaled to an activation level of 20%, 35%, 445 50%, or 65% during running at 2, 3, 4, and 5 m/s, respectively (increasingly darker 446 lines). Filled squares on each line indicate toe-off. Superimposed are plots of force 447 versus normalized fiber length and force versus ITB strain at key points in the gait cycle 448 during running at 5 m/s. Circles on the curves show where the muscle or ITB is acting at 449 that point in the gait cycle. A: TFL is longer than optimal length (L_{opt}) prior to toe-off 450 when the muscle begins to generate force. When TFL is maximally activated in early 451 swing, it operates near optimal length and stretches ITB_{ant} to its longest length in our 452 model. B: GMax3,4 is shorter than optimal length when it begins generating force in mid 453 swing and is stretched beyond optimal length in swing. When GMax3,4 is maximally 454 activated in late swing, it operates near optimal length and stretches ITB_{post} to its 455 longest length in our model.
- Figure 8. Elastic energy stored in the ITB during running at 2, 3, 4, and 5 m/s as
 predicted by the model. A: Peak energy stored in ITB_{ant} when TFL is activated 20, 35,
 50, or 65%. B: Peak energy stored in ITB_{post} when GMax is activated 20, 35, 50, or
 65%. The energy stored in GMax-ITB_{post} is calculated as the sum of energies stored in
 GMax1,2-ITB_{post1} (gray) and GMax3,4-ITB_{post2} (white).
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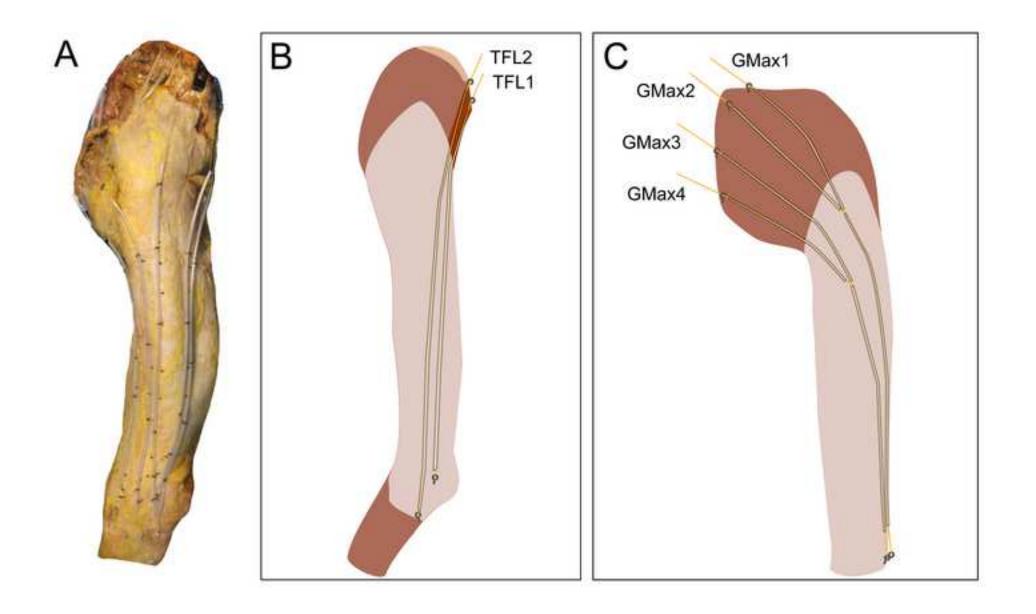
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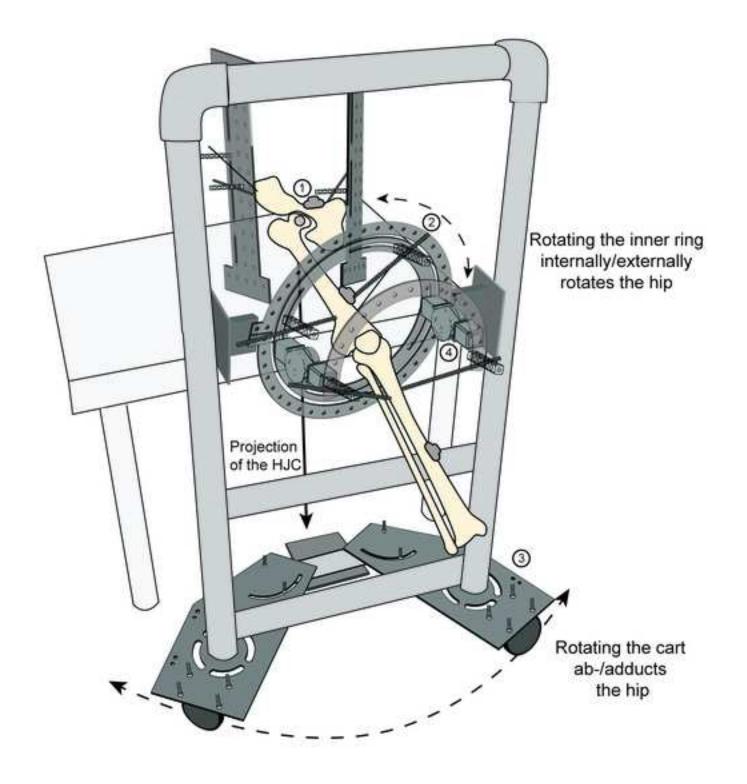
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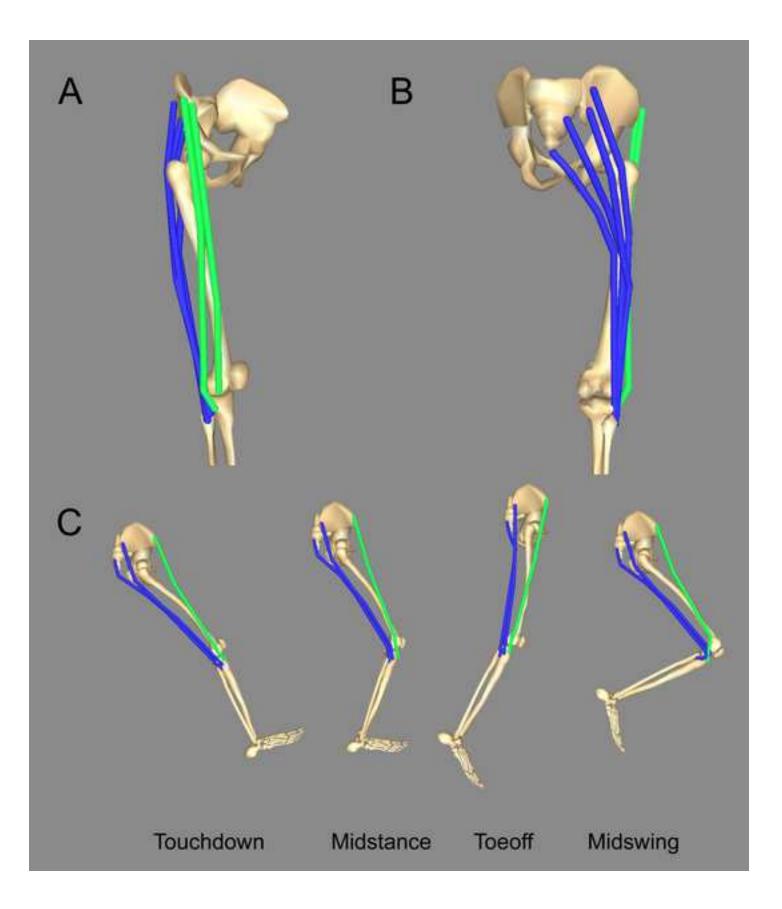
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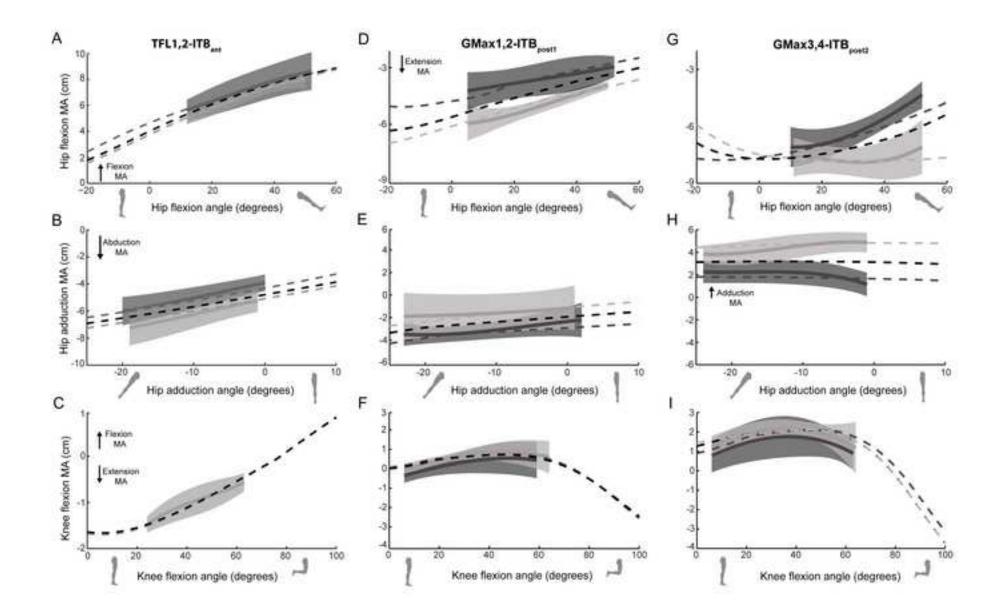
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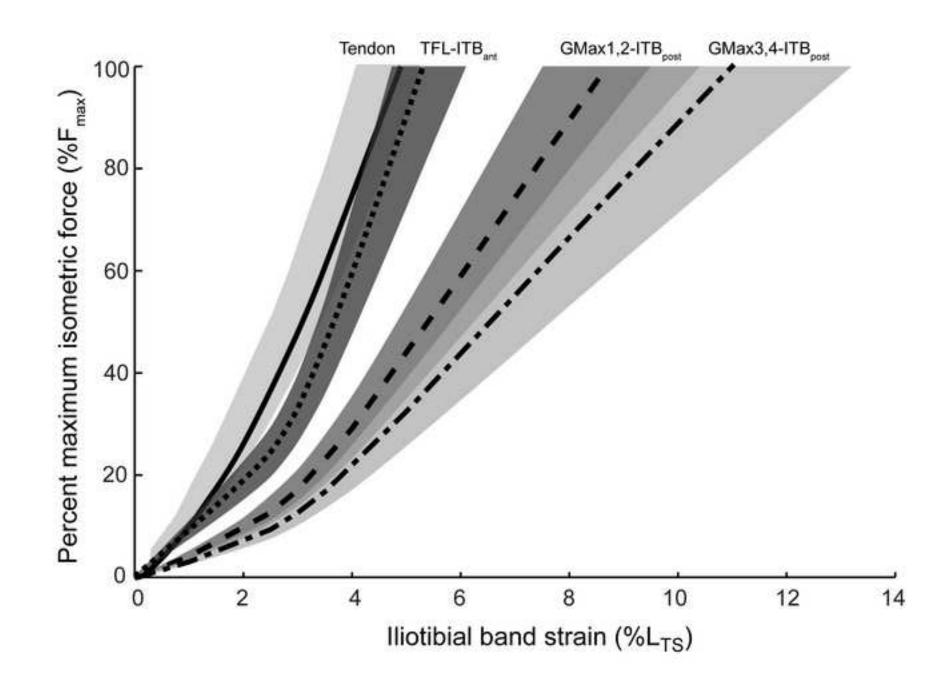
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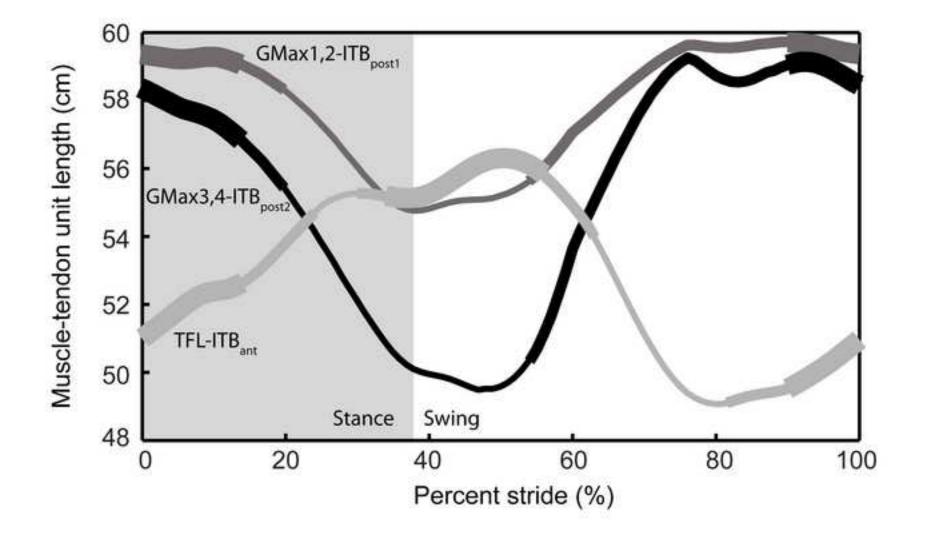
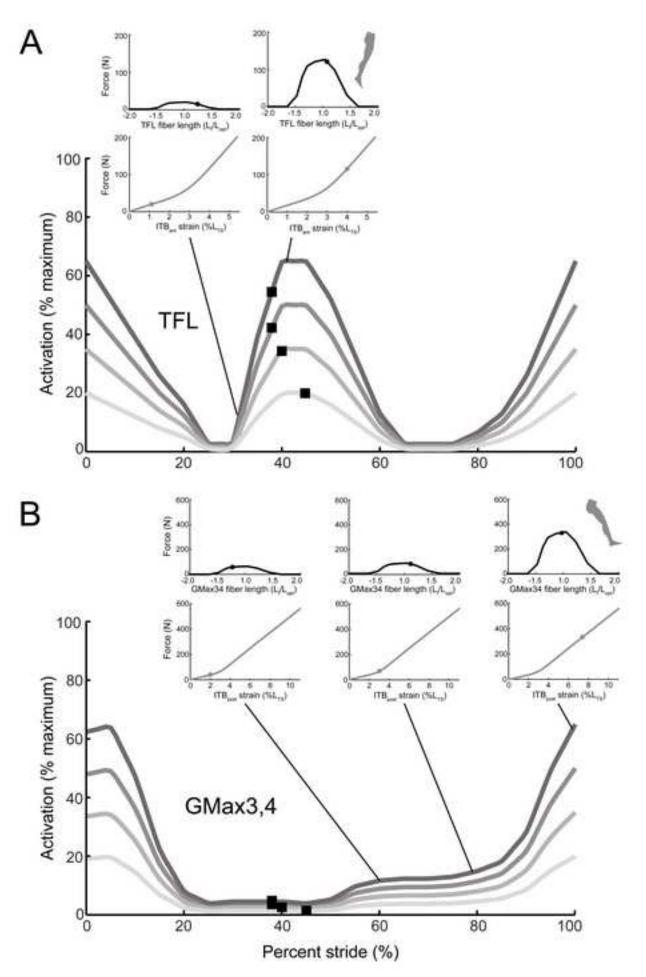
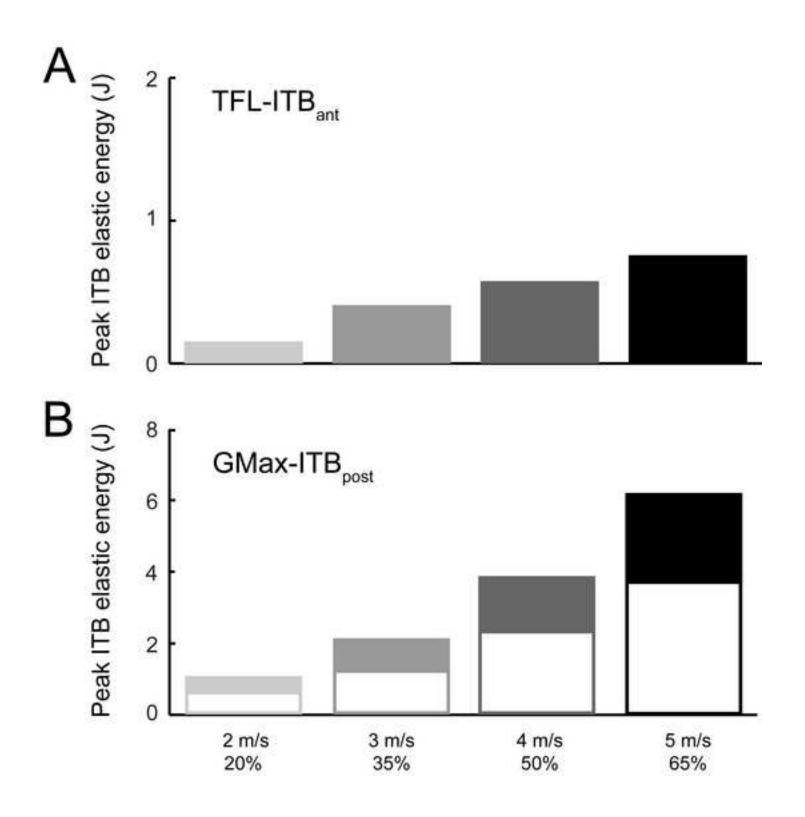
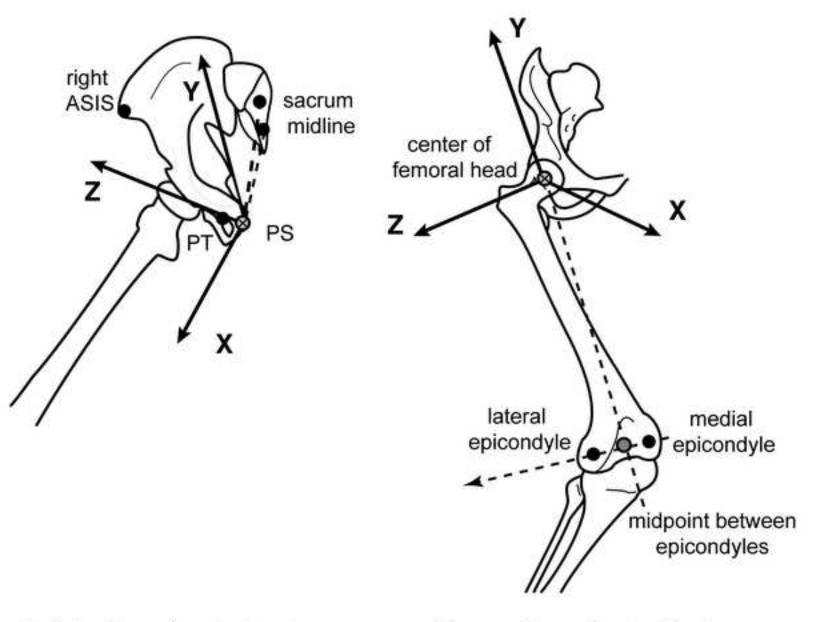


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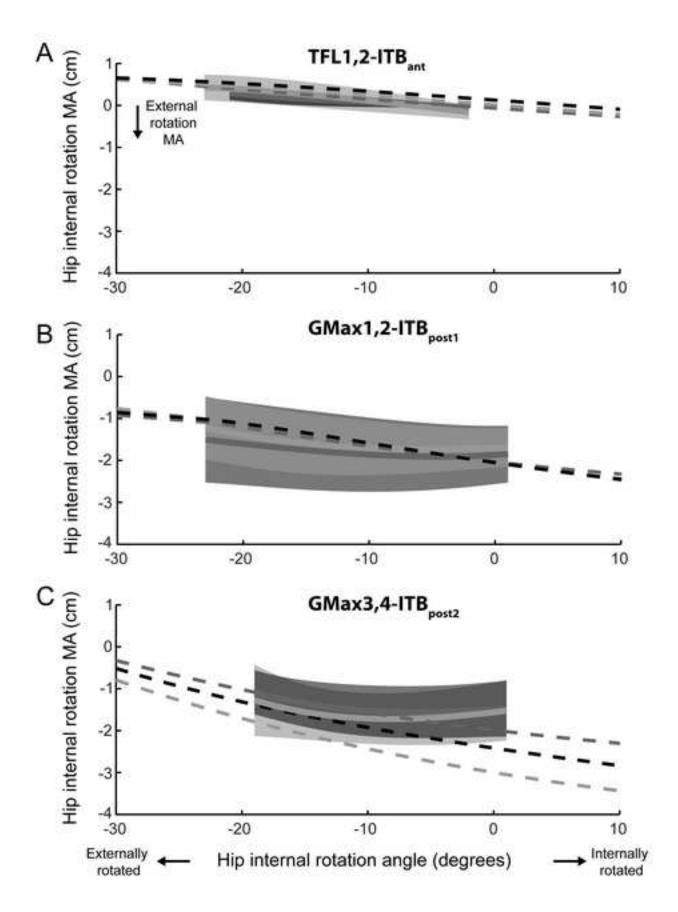




Pelvis Coordinate System

Femur Coordinate System

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Muscle	Mass (g)	Optimal fascicle length (cm)	Pennation angle (deg.)	PCSA [¥] (cm²)
TFL	35.5 ± 9.6	9.8 ± 0.7	1.1 ± 1.1	3.2 ± 1.0
GMax	412.1 ± 69.7	14.4 ± 0.7	26.3 ± 5.0	30.6 ± 5.1

Table 1. Muscle architecture of tensor fascia lata (TFL) and gluteus maximus (GMax*)

Data from 3 elderly cadaveric specimens (2 male, 1 female; mean age: 78 ± 6 years) are expressed as mean ± s.e.m. *Pennation angle is not included in the PCSA calculation since our SIMM model multiplies PCSA, specific tension, and pennation angle to determine a muscle's maximum isometric force.

Muscle	Total mass of region (g) (n=5)	Percentage of mass inserting on ITB (%) (n=2)
TFL1 [∞]	26.4 ± 7.2	100%
TFL2	21.4 ± 5.5	100%
GMax1 [¥]	110.6 ± 26.2	44.6 ± 4.9%
GMax2	109.4 ± 24.8	52.7 ± 7.8%
GMax3	121.9 ± 19.8	47.7 ± 11.3%
GMax4	104.7 ± 29.7	71.7 ± 28.3%

Table 2. Muscle regional masses of tensor fascia lata (TFL) and gluteus maximus (GMax)

Data from 5 adult males (mean age: 62 ± 10 years) are expressed as mean \pm s.e.m. ^{*}TFL was divided into two anterior-posterior regions based on origin and fascicle orientation. ^{*}GMax was separated into four superior-inferior regions.

Muscle-tendon unit	Maximum isometric force (N; <i>F_{max}</i>) [¥]	Optimal fiber length (cm; <i>L_{opt}</i>)	Pennation angle (deg; <i>θ</i>)	Tendon slack length (cm; L _{TS})
TFL1,2-ITB _{ant} \$	195.2	9.8	2.5	42.6
GMax1,2-ITB _{post1} *	455.9	15.2	26.3	42.3
GMax3,4-ITB _{post2} *	558.6	16.7	26.3	41.0

Table S1. Parameters used to scale a generic Hill-type muscle model to TFL- and GMax-ITB muscle-tendon units

^{*}TFL *PCSA*, L_{opt} , and θ and GMax PCSA and θ from our measurements. ^{*}GMax L_{opt} from Ward et al. (2009). ^{*}Fmax calculated as the product of *PCSA* and muscle specific tension of 61 N/cm² used by Arnold et al. (2010).

Table S2	
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ITB Region	Thickness (mm) [*]	Width (mm)
ITB _{ant}	0.87 ± 0.34	16.35 ± 2.03
ITB _{post1}	0.97 ± 0.12	16.85 ± 1.85
ITB _{post2}		15.33 ± 1.86

Table S2. ITB thickness and width measurements used to calculate effective cross-sectional area and stiffness of each reaion

Data from 3 elderly cadaveric specimens (2 male, 1 female; mean age: 78 ± 6 years) are expressed as mean \pm s.e.m. Thicknesses of anterior and posterior regions were measured at proximal, middle, and distal sites and averaged across sites.