Title:

Costs for integrating wind into the future ERCOT system with related costs for savings in CO$_2$ emissions

Author Affiliation:

Xi Lu
School of Engineering and Applied Science, Harvard University
Cruft Lab 211, 19 Oxford St., MA 02138

Michael B. McElroy*
School of Engineering and Applied Sciences and Department of Earth and Planetary Sciences, Harvard University
100G Pierce Hall, 29 Oxford St., MA 02138

Nora Sluzas
Department in Environmental Science & Public Policy, Harvard University
Cruft Lab 211, 19 Oxford St., MA 02138

Corresponding Author:

Michael B. McElroy (mbm@seas.harvard.edu)

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Abstract

Wind power can make an important contribution to the goal of reducing emissions of CO$_2$. The major problem relates to the intrinsic variability of the source and the difficulty of reconciling the supply of electricity with demand particularly at high levels of wind penetration. This challenge is explored for the case of the ERCOT system in Texas. Demand for electricity in Texas is projected to increase by approximately 60% by 2030. Considering hourly load data reported for 2006 assuming that the pattern of demand in 2030 should be similar to 2006 and adopting as a business as usual (BAU) reference an assumption that the anticipated additional electricity should be supplied by a combination of coal and gas with prices, discounted to 2007 dollars of $2 and $6 per MMBTU respectively, we conclude that the bus-bar price for electricity would increase by about 1.1c/kWh at a wind penetration level of 30%, by about 3.4c/kWh at a penetration level of 80%. Corresponding costs for reductions in CO$_2$ range from $20/ton to $60/ton. A number of possibilities are discussed that could contribute to a reduction in these costs including the impact of an expanded future fleet of electrically driven vehicles.

1. Introduction

It is clear, as indicated in a number of recent studies (1-3) that wind has the potential to accommodate projected global demand for electricity for the foreseeable future. Archer and Jacobson (2), using data from 7,753 surface meteorological stations complemented by results from 446 stations for which vertical soundings were available, concluded that 20% of the global potential for wind could supply as much as 14 terawatts (TW) of electricity corresponding to 7 times total current demand. Lu et al(3) using wind fields derived from assimilation of meteorological data by the NASA Goddard Earth Observing System Data Assimilation System (GEOS-5 DAS), concluded that a global network of land-based 2.5-megawatt (MW) turbines restricted to non-forested, ice-free, non-urban areas operating at as little as 20% of their rated capacity could supply
more than 40 times total current global consumption of electricity (more than 5 times consumption of energy in all forms). They concluded in particular that wind could account for the bulk of electricity consumed presently by the top 10 CO$_2$-emitting countries (countries responsible for more than 64% of total global fossil fuel related emissions) (4).

While the wind resource is more than sufficient to satisfy requirements for electricity for most of the major electricity consuming countries on an annual basis, accommodating demand or load on shorter time scales poses a more serious challenge. Wind is intrinsically variable. Real time demand for electricity is often thus poorly matched with the potential supply from wind (5). Over much of the U.S. for example, consumption of electricity tends to peak in summer responding to the requirement for air conditioning while the supply from wind is typically greatest in winter. Similarly, demand for electricity is normally greatest during the day while the potential supply from wind over land is typically highest at night in many locations.

This paper is intended to explore the implications of the potential mismatch between demand for electricity over a particular region and the supply available from wind. Costs for savings in emissions of CO$_2$ are analyzed specifically for variable levels of wind-penetration with a focus on the future, complementing earlier work directed mainly at analysis of the existing power system (6-9) that mostly focus on modeling the existing systems. We choose as a specific case for study the region of Texas served by the Electricity Reliability Council of Texas (ERCOT) which manages delivery of electricity
to 22 million consumers, accounting for 85% of demand for the state as a whole.

ERCOT is the smallest of the 3 interconnected electric grids in the United States. Largest is the Eastern interconnection accommodating requirements for 69% of the US population in the Eastern and Southern regions of the country while 23% is supplied through the Western Interconnection system. The ERCOT interconnection was selected for this study for two reasons: first, we had access to load data for the region on an hourly basis over a 5-year period; second, since wind conditions are expected to be highly correlated over the relatively limited geographic region served by ERCOT, we expect that the challenge of reconciling supply of electricity from wind with demand is likely to be more serious in this case than for either of the more extensive geographic regions served by the Eastern and Western Interconnections: low levels of wind in portions of these regions are more likely to be compensated by higher levels elsewhere (10-12).

2. Data and Methodology

The analysis will be based on a study of how different levels of wind penetration could be integrated into a system required to accommodate demand for electricity in real time on an hour-by-hour basis. We restrict attention here to five areas of west Texas, identified as Competitive Renewable Energy Zones (CREZ), selected in 2005 by the Public Utilities Commission (PUC) of Texas for preferential development of the state’s wind resources. As indicated in SI, the CREZ include some of the most favorable conditions for wind in Texas.
The analysis uses wind fields derived from reanalysis of meteorological data compiled for 2006 by the National Centers for Environmental Prediction (NCEP) of the National Oceanic and Atmospheric Administration (NOAA) (13). The data base, RUC-20, provides a record of wind speeds on an hourly basis with a spatial resolution of 20 km by 20 km. Wind speeds at 100m, the hub height for the 2.5-MW turbines considered here, were calculated on the basis of cubic spline interpolation of results for the lowest 5 layers of the record (See SI).

Results from the simulation are in excellent agreement with experience from wind farms currently operational in Texas. Approximately 2.7 GW of wind capacity was available for Texas in 2006, distributed over 13 counties in the state. Figure 1 presents a comparison of simulated and observed outputs for the system for four representative weekly intervals in 2006. The correlation between observed and simulated results for the four seasons, winter (December-February), spring (March-May), summer (June-August) and fall (September-November), amounted to 0.85, 0.73, 0.84 and 0.88 respectively with an annual mean of 0.79. The agreement is particularly impressive since the wind farms in the simulation were assumed to be distributed uniformly over the relevant counties while the actual farms were concentrated presumably in regions judged particularly favorable, and since the simulation was restricted to a study of the output of turbines with specific operational properties and capacities (2.5 MW).
Base load demand for electricity in ERCOT is supplied by a combination of nuclear and coal fired systems with load following systems fueled primarily by natural gas. In 2006, 46.3% of ERCOT electricity was produced using natural gas; coal, nuclear and wind accounted for 37.4%, 13.6% and 2.1% respectively with hydro and other minor sources responsible for the balance. The supply from wind increased by more than 200% between 2006 and 2009 (Texas now has the largest installed capacity for wind of all of the states in the U.S., reflecting in large measure the incentives introduced by the PUC in 2005 to fund connections of new systems in CREZ to the existing grid).

Future demand for electricity in the ERCOT region is projected to grow at an annual rate of approximately 2% (14). This will require an increase in generating capacity of about 60% by 2030 relative to 2006. We assume as a base case in what follows that this additional supply is produced by a price optimal combination of
coal and gas fired systems identifying this reference as the business as usual (BAU) standard against which to compare alternative models incorporating different levels of production from wind. There are two objectives for the discussion that follows: one is to identify the additional costs incurred as wind substitutes progressively for coal and gas; the second is to estimate the savings in CO₂ emissions that could be realized through a cost effective substitution of wind for coal and gas together with an estimate of the related costs. A more comprehensive analysis could attempt to account for the externality by costs (health and climate for example) associated with coal and gas. This would serve of course to enhance the advantage of wind (15, 16).

Costs for generation of electricity in the reference BAU system depend on a combination of fixed costs for capital and variable costs for operation. Capital costs are expected to be greatest for state-of-the-art coal fired systems (CFS), less for gas combined cycle systems (GCC) and lower still for gas combustion turbine systems (GCT). GCTs assumed here include reciprocating systems capable of rapid start-up. On the other hand, operational costs for CFS are lower than costs for GCC while costs for GCT are higher than costs for either CFS or GCC. A summary of cost data assumed for the different systems considered here is presented in Table 1(17) (See SI).
Table 1 Cost parameters for future coal fired systems (CFS), gas combined cycle systems (GCC) and gas combustion turbine systems (GCT), (1 mill = $ 0.001).

<table>
<thead>
<tr>
<th></th>
<th>Capital cost ($/kW)</th>
<th>Variable O&amp;M cost (mills/kWh)</th>
<th>Fixed O&amp;M cost ($/kW)</th>
<th>Heat Rate (BTU/kWh)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CFS</td>
<td>1,923</td>
<td>4.59</td>
<td>27.53</td>
<td>8,740</td>
</tr>
<tr>
<td>GCC</td>
<td>877</td>
<td>2.00</td>
<td>11.7</td>
<td>6,333</td>
</tr>
<tr>
<td>GCT</td>
<td>604</td>
<td>3.17</td>
<td>10.53</td>
<td>8,550</td>
</tr>
</tbody>
</table>

Note:

1) Financial data quoted here and elsewhere in the paper are expressed in 2007 equivalent currency values.

2) Heat rate for GCT is expressed in terms of the lower heating value (LHV); data for CFS and GCC are given in terms of the higher heating value (HHV).

3. Results and Discussion

The optimal mix of generation systems can be identified using screening curves for the different generation systems (18) as indicated in Figure 2a. The vertical axis in Figure 2a identifies the revenue required to operate a particular system for a particular number of hours over the course of a year. The horizontal axis identifies the assumed number of full-capacity operational hours for each system. The intercept for the individual curves at the zero operational hour point is determined by the combination
of the capital and fixed operational and maintenance (O&M) costs. The slope of the individual curves reflects the combination of costs for fuel, the efficiency with which this fuel can be employed to generate electricity and the expense for O&M. The analysis assumes a cost for coal of $2 per million BTU ($2/MMBTU), which may be compared with the cost of $1.6/MMBTU that pertained in 2006 (19). The cost for gas is taken as $6/MMBTU, slightly lower than the 2006 cost of $6.4/MMBTU (prices for natural gas have declined in the US since 2006 with spot prices currently closer to $4/MMBTU). The efficiency with which the energy of coal and gas can be converted to electricity is determined by the relevant heating rates, data for which are included in Table 1.

![Screening curves](image1)

Figure 2 (a) Screening curves as discussed in the text for CFS, GCC and GCT; (b) contributions from CFS, GCC and GCT required to meet the additional load demand (ALD) projected for 2030 at minimum cost.
The results in Figure 2b indicate that for CFS to be cost effective they must operate for close to 8000 full-capacity hours over the course of a year. GCC is more cost effective than CFS when the latter is operational for less than 8000 hours while GCT is most effective in meeting peak demand when operating for less than about 2400 full-capacity hours over the course of a year. The cost optimal transitions from GCT to GCC and from GCC to CFS are indicated by the vertical lines in Figure 2a.

The increase in the hourly load demand projected for 2030 is presented in Figure 2b. We assume here that the variation of additional load demand (ALD) with time in 2030 is similar to the pattern that pertained in 2006. The hourly ALD varies from a maximum of 40.6 GWh, in late summer evenings to a minimum of about 10.2 GWh, during night time hours in fall, winter and spring (See SI). In addition to the generating capacity needed to satisfy the demand as indicated in Figure 2b, the system is required to maintain a reserve sufficient to accommodate unanticipated increases in load and/or temporary losses of generating capacity. For ERCOT, this reserve is mandated at a level equal to no less than 12.5% of the total capacity of the system (5). We assume for purpose of the BAU model that this reserve is assigned to the individual components of the system (CFS, GCC and GCT) in proportion to their maximum load as indicated in Figure 2b.

The results in Figure 2b indicate that least cost production of the additional electricity in the BAU model (allowing for reserve) would require generation capacities of 15.9 GW, 10.7 GW and 19.8 GW for CFS, GCC and GCT respectively operating at CF
values of 86.8%, 50.9% and 8.2% respectively. Maximum hourly outputs for CFS, GCC and GCT are estimated at 13.8 GWh, 9.4 GWh and 17.3 GWh respectively. The average bus-bar price for electricity generated by the combined system (allowing for capacity imbedded in the reserve) is estimated at 6.2 c/kWh, reflecting prices for CFS, GCC and GCT of 5.1 c/kWh, 6.2 c/kWh and 14.8 c/kWh respectively. By way of comparison, the bus-bar price for wind-generated electricity is taken as 7 c/kWh using data for existing wind farms as reported by Wiser and Bolinger (20).

Adding wind to the generation mix results in a steepening of the duration curve for hourly load demand as indicated for the BAU case in Figure 2b. As discussed earlier, demand for electricity is greatest in summer when the supply from wind is generally at a minimum. It follows that the supply of electricity during hours of peak demand (the left hand portion of the curve in Figure 2b) must continue to be met by the conventional coal-gas system. The contribution from wind is particularly important in winter when demand is at a seasonal minimum (impacting thus differentially the shape of the residual coal-gas curve to the right of the demand curve in Figure 2b). As the supply of power from wind increases, the economic advantages of the source from CFS decrease. The resulting change in the mix of wind, CFS, GCC and GCT as constrained to supply electricity at minimum additional cost is illustrated in Figure 3a. Coal drops out of the mix as the penetration of wind increases above 30% on an annual basis. Requirements for standby gas systems to accommodate temporal deficiencies in the supply from wind increase accordingly adding additional expense to the system due to the resulting lower
CF of the gas system. For penetration levels of wind greater than about 30%, the source of power from wind is more than sufficient to meet demand, as indicated in the figure, resulting in a potential net increase in the supply of electricity relative to demand.

Increasing penetration of wind results in additional uncertainty in the power required to be supplied by the coal-gas system. Reserves must be increased accordingly: the higher the wind penetration, the greater the need for reserves to accommodate unanticipated shortfalls in the supply from wind. As discussed in SI, this reserve is estimated to increase from 12.5% in the low-wind BAU limit to as much as 30% at a wind penetration level of 80%.

Addition of wind to the generation mix results in a decrease in emissions of CO$_2$ relative to BAU. The reduction in emissions is particularly significant at lower levels of wind penetration responding to differential displacement of coal relative to gas. At a penetration level of 30%, wind is predicted to result in a 58.0% reduction of emissions of CO$_2$ (equivalent to 81.2 million tons of CO$_2$ per year). Reductions continue as coal is eliminated but at a slower rate reflecting the lower CO$_2$ emission factors for GCC as compared to CFS. Emissions of CO$_2$ as a function of wind penetration corresponding to the data in Figure 3a are presented in Figure 4a.

(a) Price Optimal
Figure 3 Changes in the mix of power generation as a function of wind penetration level. For further discussion of the price and CO$_2$ optimal models, see text.

The results in Figures 3a and 4a were constrained to minimize the additional cost for electricity relative to BAU resulting from increasing penetration of wind. An alternate strategy would seek to identify the most cost effective way to maximize reductions in CO$_2$. A displacement to the right of the GCC/CFS transition in Figure 2b would result in a decrease in CFS relative to GCC with a corresponding reduction in emissions of CO$_2$. The net cost for electricity would increase however since production from GCC is more expensive than production from CFS. There is an optimal
displacement that would ensure maximum reduction of CO\textsubscript{2} emissions at minimum cost. The resulting change in the mix of generation sources as a function of wind penetration for this least cost CO\textsubscript{2} reduction scenario is presented in Figure 3b. The corresponding change in emissions is illustrated in Figure 4b. Emissions would be reduced by as much as 50.6\% at a wind penetration level of 20\%, significantly larger than the reduction of 35.8\% for the same penetration level in the price optimal model. The primary difference between the results in Figures 4a and 4b reflects the more rapid transition from CFS to GCC in the CO\textsubscript{2} optimal model as compared to the price optimal model. Costs for CO\textsubscript{2} reductions for the price optimal model and the CO\textsubscript{2} optimal model are presented as functions of wind penetration in Figure 5a.
Figure 4 Changes in emissions of CO$_2$ from CFS, GCC and GCT as a function of wind penetration level. Reductions in emissions are illustrated in yellow. For further discussion of the price and CO$_2$ optimal models, see text.

Since the cost for electricity delivered by wind (7c/kWh) is higher than the cost for power delivered either by coal or gas fired systems at low penetration levels for wind, the cost for electricity rises inevitably as wind begins to displace coal and gas. The increase in cost for the price optimal model is summarized in Figure 5b. The increase amounts to 0.71 c/kWh at a wind penetration level of 20% rising to 1.1 c/kWh at a penetration level of 30%. The cost for the CFS, GCC and GCT components at a wind penetration level of 20% average 5.29 c/kWh, 6.06 c/kWh and 15.07 c/kWh respectively. The increase in cost for the CFS (relative to the BAU reference of 5.14 c/kWh) reflects a reduction in the number of operational hours for this system. The decrease in the cost for power supplied by GCC at 20% wind relative to BAU (0.15 c/kWh) is attributable to the increase in CF for this component as coal is replaced selectively by gas. Coal ceases to be important when the wind penetration level rises above 30%. The prices for the GCC and GCT components at the 30% wind penetration
level are equal to 6.01 c/kWh and 15.32 c/kWh respectively. Costs for electricity in the CO₂ optimal model are only slightly higher than the costs for the price optimal model (less than 0.024 c/kWh), too small to be resolved on the trend curve displayed in Figure 5b.

![Figure 5](a) Cost for CO₂ savings as a function of wind penetration level for the price and CO₂ optimal models. (b) System wide bus-bar price of electricity as a function of wind penetration level. Results for the price optimal and CO₂ optimal models are indistinguishable given the resolution of the curve displaced.
The estimates presented here for the costs related to the introduction into the 2030 ERCOT electricity system of different levels of wind depend obviously on the assumptions made concerning the expense for future coal and gas systems and for proposed new wind systems. Future (2030) prices for coal and gas were taken equal to $2/MMBTU and $6/MMBTU respectively. Projections of future prices for either coal or gas are subject however to significant uncertainty. Spot prices for natural gas, for example, have varied from a high of close to $14/MMBTU to a low of less than $4/MMBTU over the past 5 years (21). Adding to the ambiguity relating to market related factors is the uncertainty associated with the possible introduction of a future tax on emissions of CO2. It is much easier to project costs for wind systems. We assumed here that electricity could be generated in 2030 using wind at a bus-bar price of 7 c/kWh reflecting experience with recent wind installations (20, 22). It could be argued however that with economies of scale, capital costs for wind systems might be expected to decline in the future. If costs for coal and gas should rise relative to the estimates assumed here and if prices for wind systems should decline (both possibilities judged as not unlikely), the expense for incorporation of wind in the future ERCOT system could switch readily from positive to negative.

As indicated in Figure 3, the quantity of electricity that could be generated using wind at high penetration levels (levels greater than about 40%) could potentially exceed projected demand. We assigned zero value to this excess in the analysis presented above. It could be used, however, with electrolysis to produce H2, which could serve as
a feedstock for production of nitrogen fertilizer, for methanol that could substitute for gasoline and diesel fuels in the transportation sector, or for a host of other useful chemical products (23-25). The problem is that since the supply of H₂ contributed by the potential excess in electricity from wind would be necessarily intermittent, the costs associated with the electrolysis system would be prohibitive if the electrolysis system were supplied solely by the electricity from excess wind: the capacity factor for the electrolysis system would be necessarily very low. This complication could be avoided if electricity from conventional sources, specifically gas and nuclear, in addition to that from excess wind could be channeled to supply the demands of the projected electrolysis system. Further study to explore the feasibility of such an initiative, including its impact on the overall costs of electricity and the potential to accommodate further savings in emissions of CO₂, would clearly be of value.

There are 11.5 million conventional gasoline and/or diesel powered motor vehicles registered currently in the state of Texas (26). Given present trends, it is likely that a significant fraction of the future (2030) motor vehicle fleet not only in Texas but also in the U.S. more generally will be powered at least in part by electricity. The battery pack of the Chevrolet Volt introduced recently by General Motors has the potential to store up to 8.8 kWh of useful energy (27). If we assume that 20% of the current vehicle population could be represented by plug-in hybrids (PHEVs) or E-REVs by 2030, the batteries of these vehicles would have the capacity to store up to 20 GWh of electricity, with the potential to generate important savings not only in the demand for oil but also in
emissions of CO₂ and to do so with a significant reduction in the cost of motoring.

To explore the potential benefits of a future fleet of PHEVs, we repeated the analysis of the electrical system described here assuming 2.25 million PHEV vehicles with properties similar to those advertised for the Chevrolet E-REV. We assumed that these vehicles would be charged at night when demand for electricity would normally be at a minimum, that individual vehicles would undergo a typical charge-discharge cycle over a 24-hour period (28-29) and that 30% of the electricity stored in the vehicle battery packs could be returned to the grid during times of high demand during the day. This would result in an increase in the operational efficiency of the overall electrical system by smoothing out the normal differences in day/night demand for power, taking advantage further of the fact that the supply of electricity from wind is typically greater at night than during the day. The benefits of the proposed PHEV fleet would be particularly significant at higher levels of wind penetration. At a penetration level for wind of greater than 60%, introduction of the proposed PHEV fleet could reduce the cost for CO₂ savings by as much as $1.8 per ton, with minimal impact on the overall cost for electricity (See SI).

This study assumed that the hourly variation in the growth of demand for electricity projected for ERCOT in 2030 should be similar to the pattern observed in 2006. It assumed further that the wind resources derived here for 2006 should apply at least approximately to conditions expected in the future (i.e. no significant change with time in either the strength or temporal/spatial variation of wind). As discussed earlier,
our analysis is sensitive also to the specific assumptions made with respect to future prices not only for coal and gas but also for wind systems. An analysis of the sensitivity of results to assumptions concerning fuel prices, interest rates and targeted IRR is presented in SI.

Wind resources tend to peak in winter and at night when demand for electricity is typically at a minimum. A combination of wind and solar generated electricity would provide a better match of supply to demand \((15, 16)\). The advantage of the complementarity between wind and solar would be offset however to some extent by the fact that solar source is currently more expensive than the source from wind. We propose to explore this issue further in a future study.
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Description of SI section:

Potential hourly production of electricity from wind in the CREZ region of Texas is evaluated using assimilated meteorological data provided by NCEP. An economic model is applied to derive costs for incorporation of different levels of wind power in projected 2030 demand for electricity in Texas.
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