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Blast-induced phenotypic switching in cerebral vasospasm

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Vasospasm of the cerebrovasculature is a common manifestation of blast-induced traumatic brain injury (bTBI) reported among combat casualties in the conflicts in Afghanistan and Iraq. Cerebral vasospasm occurs more frequently, and with earlier onset, in bTBI patients than in patients with other TBI injury modes, such as blunt force trauma. Though vasospasm is usually associated with the presence of subarachnoid hemorrhage (SAH), SAH is not required for vasospasm in bTBI, which suggests that the unique mechanics of blast injury could potentiate vasospasm onset, accounting for the increased incidence. Here, using theoretical and in vitro models, we show that a single rapid mechanical insult can induce vascular hypercontractility and remodeling, indicative of vasospasm initiation. We employed high-velocity stretching of engineered arterial lamellae to simulate the mechanical forces of a blast pulse on the vasculature. An hour after a simulated blast, injured tissues displayed altered intracellular calcium dynamics leading to hypercontractility and remodeling, indicative of vasospasm initiation. These results suggest that an acute, blast-like injury is sufficient to induce a hypercontraction-induced genetic switch that potentiates vascular remodeling, and cerebral vasospasm, in bTBI patients.

Results

Simulated Blast in Engineered Arterial Lamellae. A pressure pulse in an artery would primarily manifest as acute circumferential stretching caused by luminal expansion. To mimic this deformation, we developed engineered arterial lamellae (Fig. 1A) composed of a highly aligned monolayer of VSMCs (Fig. 1B) on an elastic substrate, which were exposed to a simulated blast consisting of a single axial high-velocity stretch (Fig. 1C, Movie S1). Due to the viscoelasticity (21) and strain stiffening (22) of arterial tissues, as well as the incompressibility of the surrounding brain tissue and cerebrospinal fluid (23), we assumed that the blast would result in a rapid, but low-magnitude strain. We therefore applied simulated blast at 5% and 10% strain at a strain rate of 1,000% strain/s (Fig. 1D, Movie S2). Evidence of acute and chronic vasospasm were measured 1–24 h postblast. Simulated blast did not cause obvious trauma such as altered tissue architecture (Fig. 1E), cell density, induced membrane poration, or increased apoptosis (Fig. S1).

Simulated Blast Induces Elevated Cytosolic Calcium Transients. Recently, a study of controlled cortical impact injury in the rat demonstrated a reduced lumen diameter in the pial arterioles 1 h after injury, coincident with a reduction in ipsilateral cerebral blood flow (24). Subsequently, an additional study suggested L-type Ca²⁺ blockade would restore cerebral vasoreactivity fol-


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Following lateral fluid percussion injury in rats (25). We asked if in our experimental model of blast-induced vascular injury, disrupted Ca\textsuperscript{2+} dynamics may play a role in initiating changes in vascular tone by contributing to the hypercontractility characteristic of acute vasospasm (26). We measured the temporal changes in cytosolic Ca\textsuperscript{2+} levels, or transients, in the engineered tissues 1 h after simulated blast (Fig. 1 F, Movie S3). Endothelial injury following TBI can affect endothelin-1 (ET-1) production (16), and elevated cerebral spinal fluid levels of ET-1 have been implicated in cerebral vasospasm (27, 28), so we measured ET-1 induced calcium transients as well as spontaneous transients. Tissues exposed to simulated blast had transients with higher and more prolonged peaks following ET-1 stimulation than did control tissues (Fig. 1 G and H). This trend was also apparent for spontaneous transients (Fig. 1 I). This elevated response suggests that blast mechanics predispose VSMCs to hypercontraction through increased Ca\textsuperscript{2+} uptake and may act synergistically with elevated ET-1 levels to accelerate vasospasm.

**Simulated Blast Induces Dysfunctional Contractile Dynamics.** To characterize the functional effect of simulated blast, we measured contractile stress generation using a vascular muscular thin film (vMTF) assay (19, 20). The vMTFs are biohybrid constructs composed of a layer of polydimethylsiloxane (PDMS) and a layer of micropatterned VSMCs. When the muscle contracts, it bends the passive PDMS film whose curvature can be measured and used to calculate the tissue stress (Fig. 2 B). The vMTFs were released from the stretchable substrate (Fig. 2 A) and the temporal change in curvature (Fig. 2 C, Movie S4) and tissue stress (Fig. 2 D) were measured during stimulation with ET-1 and rho kinase (ROCK) inhibitor HA-1077, allowing characterization of the basal tone and contractility of the tissue (Fig. S2).

An hour after simulated blast, tissues exhibited nearly twofold increases in ET-1 induced contraction (Fig. 2 E), consistent with the observed elevated Ca\textsuperscript{2+}, but no change in basal contractile tone (Fig. 2 F). To test whether stress during the blast is responsible for this hypercontraction, we inhibited ROCK prior to simulated blast, to relieve cytoskeletal contractile tension during the blast. This stress relief during the blast mitigated the ET-1 hypersensitivity (Fig. 2 G) with no change in basal tone (Fig. 2 H), suggesting that cytoskeletal mechanical tension during blast contributes to postblast hypercontractility.

Because vasospasm is a chronic dysfunction, we also tested tissue function 24 h after simulated blast. At this later time point, mildly and severely injured tissues showed markedly different contractile dynamics (Fig. 2 I and J). Tissues strained 5% remained hypersensitive to ET-1 stimulation, though at a decreased level, 1 h after blast (Fig. S3), but that...
All graphs: mean ± SEM.

Normalized ET-1 induced contraction and basal tone 1 h after simulated blast for tissues pretreated with ROCK inhibitor. (Fig. 2A) vMTFs were serially stimulated with ET-1 and HA-1077. (C-D) vMTFs were serially stimulated with ET-1 and HA-1077. (C) Single vMTF during experimental protocol. (Scale bar, 1 mm). (D) Temporal change in vMTF stress due to serial stimulation, 1 h after simulated blast. (E-F) Normalized ET-1 induced contraction and basal tone 1 h after simulated blast. (G-H) Normalized induced contraction and basal tone 1 h after simulated blast for tissues pretreated with ROCK inhibitor. (I-J) Normalized induced contraction and basal tone 24 h after simulated blast. (K-L) Normalized induced contraction and basal tone 24 h after simulated blast for tissues treated ROCK inhibitor immediately following the blast. All graphs: mean ± SEM.

Dynamic Phenotype Switching Predicts Long-Term Contractility and Stress Remodeling. Given the reduction in contractile stress at 24 h in the severely injured tissues with respect to both control and mildly injured tissues, we reasoned that severely injured tissues were remodeling their stress state by changing the phenotype of a subpopulation of the VSMCs in the blast-induced hypercontractile tissues. We developed an elasticity-based computational model, based on previous models of stress-induced growth and remodeling (31, 32), to better understand how blast-induced hypercontraction potentiates chronic contractile variation between mildly and severely injured tissues.

Stress Remodeling. Given the reduction in contractile stress at 24 h in the severely injured tissues with respect to both control and mildly injured tissues, we reasoned that severely injured tissues were remodeling their stress state by changing the phenotype of a subpopulation of the VSMCs in the blast-induced hypercontractile tissues.
preblast equilibrium (Fig. 3 B–E); however, during early vasospasm development (e.g., 24 h postblast), the model qualitatively reproduces the experimentally observed contractility (Fig. 3 F and G, see Fig. 2 I and J for comparison) and predicts that mild injury induces a slightly more contractile population, while the more severe injury induces a more synthetic population (Fig. 3H). Phenotypic switching in VSMCs is necessary to maintain SAH induced vasospasm (35). Our model predicts that in bTBI vasospasm, stress-induced phenotype switching may drive postblast remodeling.

Simulated Blast Induces Dynamic Phenotype Switching in VSMCs. To test in vitro whether blast forces can lead to phenotypic switch, we measured protein (Fig. 4 A and B) and mRNA (Fig. 4C) expression of two primary markers of contractile VSMCs, smooth muscle myosin heavy chain (SM-MHC) and smoothelin, 24 h after exposure to simulated blast. Tissues exposed to 5% strain exhibited nonsignificant increased SM-MHC transcripts but little change in smoothelin expression (Fig. 4 A–C), while severe (10% strain) simulated blast decreased expression of smoothelin (Fig. 4 A and B) and decreased mRNA expression of both markers (Fig. 4C). These data suggest that acute mechanical injury can potentiate a switch away from the contractile phenotype in VSMCs, as theoretically predicted. Further, if postblast tissue contraction is inhibited, contractile marker expression is unchanged in blasted tissues (Fig. 4D). These results demonstrate that mechanotransduced hypercontraction, due to acute mechanical injury, facilitates hastened VSMC phenotype switching, potentially accounting for accelerated onset of vasospasm in bTBI patients.

Discussion
Vascular injury is an oft overlooked component of traumatic brain injury. But, local ischemia resulting from acute vasospasms may play a significant role in the delayed onset of clinical manifestations of bTBI. The normal progression of cerebral vasospasm is an initial hypercontraction (26) followed by vessel remodeling (4–6) and narrowing (9). Here, we find that within 24 h of blast-like injury, mechanotransduction of extreme mechanical forces can induce both hypercontractility and phenotypic switching indicative of the onset of remodeling.

Our theoretical model suggests that these phenomena are related by the stress-induced remodeling pathways that endow the vasculature with its robust mechanoadaptability (32, 34). Specifically, these results suggest that blast-induced hypercontraction leads to elevated tissue stress, which can, in cases of severe injury, induce maladaptive compensatory remodeling, facilitated by phenotype switching. The expression of contractile phenotype markers and the variable contractility suggests that in the 10% strain-injured tissue, there is a mixed population of hypercontractile and synthetic VSMCs.

The relief of short-term hypercontractility and long-term phenotype switching with inhibition of ROCK suggests that cytoskeletal tension and forces on integrins are playing a key role in vasospasm initiation. Integrins are the primary transducers of mechanical force to the cell’s cytoskeleton (36, 37), and integrin stimulation is involved in a wide range of cellular signaling, including altering calcium dynamics (11, 12) and phenotypic behavior (38–40) in VSMCs. The mechanical loading of the blast and the resulting hypercontractility both likely result in abnormal integrin stimulation, potentially mediating the observed vasospasm behavior.

While this study has focused on the effect of acute stretch on in vitro engineered arterial lamellae, in vivo the cerebrovasculature is exposed to a complex milieu of signals that are not accounted for in our model. The mechanotransduction pathways identified here likely act in concert with, for example, dysfunctional endothelial behavior (16) and SAH (7) to accelerate vasospasm onset in bTBI patients. Moreover, the cerebrovasculature is exposed to dynamically varying mechanical forces, such as delayed hypotension (17), that could also have an additional mechanotransductive effect on vascular remodeling.

As a result of the conflicts in Afghanistan and Iraq, the number of bTBI patients, for whom there are few effective therapies (41), is rising rapidly. To better understand how to treat these patients, it is important to understand the source and pathway of their dysfunction. Here, we identify a unique source of cerebral vasospasm; blast-induced mechanotransduced vasospasm independent of SAH. These results suggest that bTBI vasospasm may require different therapeutic strategies than those currently employed for SAH induced vasospasm.

Methods
Experimental methods are briefly described, a detailed description is provided in SI Text.

Tissue Construction. Tissues were patterned using microcontact printed (42) 10 μm wide lines separated by 10 μm wide gaps. VSMCs were seeded at 25,000 cells/cm², creating a confluent tissue. High-velocity acute uniaxial stretch (43, 44) was applied using a linear motor to displace one end of a 5 × 8 cm elastomer membrane while holding the other end fixed. The strain field (Fig. 1D) of the substrate was verified using high-speed video and a three-point strain algorithm (45).

Calcium Measurement. To measure cytosolic calcium, Fluo-4 AM calcium indicating dye was added to culture for 15 min and the culture was allowed to equilibrate for 15 min post wash out. Fluorescent intensity was measured 1 frame/s for 10 min to acquire spontaneous transients and 20 min following

![Image](https://www.pnas.org/cgi/doi/10.1073/pnas.1105860108 Alford et al.)
ET-1 treatment. Normalized temporal intensities of individual regions were registered by onset time to determine the mean curves in Fig. 1.

Tissue Stress Measurement. VMTF were constructed as previously published (19). The VMTF tissue stress was calculated as previously published (20). To inhibit ROCK during blast, tissues were treated with 100 μM HA-1077 for 30 min prior to simulated blast and immediately washed out following blast. To inhibit postblast ROCK activity, tissues were treated with 10 μM HA-1077 immediately following simulated blast. HA-1077 was washed out 30 min prior to VMTF experiments. Substrate and tissue thicknesses necessary for stress measurement were measured using stylus profilometry and confocal microscopy, respectively (Fig. 54).

Theoretical Model. The model methods are presented briefly here, and in more extensive detail in SI Text, Figs. S5, S6, S7, and S8.

We employ finite elastic growth theory (46) adapted for pseudocontracture (47) to model the evolution of stress in the tissue. Within this framework, Cauchy stress \( \tau \) is considered a function of elastic stretch ratio \( F_a \) such that

\[
\sigma = F_a - \frac{\partial \mathcal{W}(F_a)}{\partial F_a} - \mathcal{P}. \tag{[1]}
\]

where \( \mathcal{W} \) is the strain-energy density function, and \( \mathcal{P} \) is a Lagrange multiplier. \( F_a \) is a component of the total deformation (\( F \)) which is also composed of the remodeling deformation \( (F_g = \text{diag}(\gamma_1, 1, 1)) \), and active deformation \( (F_a = \text{diag}(\gamma_2, 1, 1)) \), which represent the change in the zero-stress configuration due to remodeling and contraction, respectively. \( \gamma \) is the stretch ratio representing the stress-free shortening that the tissue would undergo if it was unconstrained. Total deformation is defined as

\[
F = F_a - F_g \tag{[2]}
\]

The tissue is composed of a mixed population of contractile and synthetic cells and is treated as a constrained mixture (48) of both cell types. Total tissue tension and remodeling rate are dependent on the fraction of the population of each cell type, with synthetic cells being noncontractile (\( \lambda_a = 1 \)), but remodeling more quickly. The total stress is given by

\[
\sigma = \phi_1 c \sigma_a + \phi_\lambda \sigma_c \tag{[3]}
\]

where \( \phi_i \) and \( \phi_\lambda \) are the fraction of total cells expressing contractile or synthetic phenotypes, respectively and \( \phi_1 + \phi_\lambda = 1 \). We assume that the tissue grows to reequilibrate both tissue stress and the rate of remodeling \( \lambda_a \) is given by

\[
\lambda_a = \frac{\phi_1}{\phi_\lambda} \left( \sigma_a - \sigma_c \right) + \frac{\phi_\lambda}{\phi_1} \left( \lambda_a - \lambda_c \right). \tag{[4]}
\]

where \( \lambda_c \) is the tissue’s target stress and \( \tau_a \) and \( \tau_c \) are time constants (32, 33, 49). We further assume that perturbation from the target stress results in a change in the phenotype population, with small perturbations inducing a more contractile population and large perturbations causing the population to become more synthetic. We characterize this phenotype switching by the rate of change of contractile population fraction \( \phi_i \) given by

\[
\frac{\dot{\phi}_i}{\phi_i} = -\frac{1}{\tau_{\phi_i}} \left( -1 \frac{\sigma_a - \sigma_c}{\gamma_\sigma} + 2 \frac{\sigma_c - \sigma_a}{\gamma_\sigma} \right) + \frac{1}{\tau_{\phi_i}} (\phi_\lambda - \phi_i). \tag{[5]}
\]

where the first term represents the influence of stress perturbation on phenotype and the second is a corrective term that acts to bring the phenotype distribution back to equilibrium. \( \gamma \) is a constant that depends on the degree of hypercontraction, assumed to be proportional to the blast severity (Fig. 3A), \( \beta \) is a time constant and \( \tau \) is time after blast. In response to the perturbed contractile stress, the tissue temporally remodels and undergoes phenotype switching to reequilibrate the tissue tension.

To simulate the VMTF experiments, induced contraction and basal tone are calculated by setting \( \dot{\lambda}_a = 0.6 \) (fully contracted) and \( \dot{\lambda}_a = 1 \) (fully relaxed) respectively, and comparing the resulting stress to the unstimulated tissue.

Biochemistry. Western blotting and RT-PCR were performed using standard methods detailed in the online supplement.

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