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# Parallel microfluidic synthesis of size-tunable polymeric nanoparticles using 3D flow focusing towards *in vivo* study

Jong-Min Lim, PhD<sup>a,b,c</sup>, Nicolas Bertrand, PhD<sup>c</sup>, Pedro M. Valencia, PhD<sup>d</sup>, Minsoung Rhee, PhD<sup>a,b,c</sup>, Robert Langer, ScD<sup>c,d</sup>, Sangyong Jon, PhD<sup>e</sup>, Omid C. Farokhzad, MD<sup>b,\*</sup>, and Rohit Karnik, PhD<sup>a,\*</sup>

<sup>a</sup>Department of Mechanical Engineering, Massachusetts Institute of Technology, Cambridge, MA, USA

<sup>b</sup>Laboratory of Nanomedicine and Biomaterials, Department of Anesthesiology, Brigham and Women's Hospital - Harvard Medical School, Boston, MA, USA

<sup>c</sup>David H. Koch Institute for Integrative Cancer Research, Massachusetts Institute of Technology, Cambridge, MA, USA

<sup>d</sup>Department of Chemical Engineering, Massachusetts Institute of Technology, Cambridge, MA, USA

<sup>e</sup>Department of Biological Sciences, KAIST, Daejeon, Republic of Korea

#### Abstract

Microfluidic synthesis of nanoparticles (NPs) can enhance the controllability and reproducibility in physicochemical properties of NPs compared to bulk synthesis methods. However, applications of microfluidic synthesis are typically limited to *in vitro* studies due to low production rates. Herein, we report the parallelization of NP synthesis by 3D hydrodynamic flow focusing (HFF) using a multilayer microfluidic system to enhance the production rate without losing the advantages of reproducibility, controllability, and robustness. Using parallel 3D HFF, polymeric poly(lactide-*co*-glycolide)-*b*-polyethyleneglycol (PLGA-PEG) NPs with sizes tunable in the range of 13–150 nm could be synthesized reproducibly with high production rate. As a proof of concept, we used this system to perform *in vivo* pharmacokinetic and biodistribution study of small (20 nm diameter) PLGA-PEG NPs that are otherwise difficult to synthesize. Microfluidic parallelization thus enables synthesis of NPs with tunable properties with production rates suitable for both *in vitro* and *in vivo* studies.

#### Keywords

Nanoparticles; Nanoprecipitation; 3D flow focusing; Microfluidics; Block copolymers

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<sup>&</sup>lt;sup>\*</sup>Corresponding authors: ofarokhzad@zeus.bwh.harvard.edu (O.C. Farokhzad), karnik@mit.edu (R. Karnik).

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#### Introduction

Polymeric nanoparticles (NPs) have shown great promise as nanocarriers for drug delivery.<sup>1–3</sup> NPs made of poly(lactide-*co*-glycolide)-*b*-polyethyleneglycol (PLGA-PEG) block copolymers are particularly appealing as nanomedicines because they are biodegradable and biocompatible, have the ability to incorporate chemical moieties including drug molecules and targeting agents, and can controllably release their payload.<sup>4–6</sup> Indeed, targeted PLGA-PEG NPs for prostate cancer therapy have successfully completed Phase I clinical trials and are poised to impact human health.<sup>7</sup>

However, the translation of NPs to the clinic faces several challenges, with the majority of the NPs not making it beyond the proof-of-concept stage.<sup>8,9</sup> Major issues include the extensive in vitro and in vivo screening and optimization required, and the batch-to-batch variability in manufacture of NPs. While polymeric NPs are typically synthesized in bulk by the nanoprecitipation/solvent exchange method or by emulsification using surfactants, microfluidic platforms offer reaction environments that are precisely controlled at the microscale. As a result, microfluidic platforms have been recently adopted for the synthesis of NPs in a more controllable and reproducible manner.<sup>9–12</sup> Microfluidic platforms also allow systematic tuning of the biophysicochemical properties of NPs, facilitating their screening and optimization.<sup>8,9,13–16</sup> We have demonstrated the controlled synthesis of PLGA-PEG NPs by rapid and tunable mixing in microfluidic platforms known as 2D hydrodynamic flow focusing (HFF) and 3D HFF.<sup>13,17</sup> 3D HFF isolates the precipitating polymers from microchannel walls and eliminates microchannel clogging, which has enabled reproducible synthesis of monodisperse NPs with tunable sizes from 30-230 nm. Synthesis of lipid NPs using rapid mixing in microfluidic channels by microvortices and herringbone microstructures has also been reported.<sup>18-20</sup>

Despite these advances, the role of microfluidic platforms in the development of drug delivery systems faces some challenges. While *in vitro* studies require small amounts of NPs (e.g., ~50 µg/well), subsequent *in vivo* studies require significantly larger amounts (e.g., ~5 mg/mouse). Mixers that are suitable for larger-scale synthesis<sup>18,21</sup> are not well-suited for creating a library of NPs for *in vitro* screening. In devices such as 3D HFF that are well-suited for *in vitro* screening of NPs, modifying the experimental procedures to increase the yield drastically affects the physicochemical properties of NPs. For example, changing the platform's architecture to tolerate higher internal pressure affects the mixing time and the physicochemical properties of the NPs. Therefore, parallelization of the microchannels is a promising way to meet the NP production yields required for *in vivo* studies; such parallel process approaches have been studied for emulsion droplet generation<sup>22–27</sup> and in the chemical engineering industry.<sup>28</sup>

Herein, we report parallel synthesis of NPs using a multilayer microfluidic system to enhance the production yield without losing the advantages of reproducibility, controllability, and robustness of 3D HFF. The relevance of this novel microfluidic design for the development of PLGA-PEG NPs was assessed by synthesizing NPs in the range of 13–150 nm with high production rates. We show that NPs produced at high production rates have identical properties as those prepared with single stream channels. Finally, as a proof of concept, we performed *in vivo* pharmacokinetic (PK) and biodistribution study using PLGA-PEG NPs rapidly synthesized by the parallel 3D HFF. This parallel microfluidic system extends the range of applications of HFF for controlled synthesis of NPs with tunable properties from *in vitro* to *in vivo* studies.

#### Methods

#### Fabrication of multilayer poly(dimethylsiloxane) (PDMS) microfluidic device

Multilayer 3D HFF microfluidic device was prepared using multilayer photolithography and multilayer soft lithography. Master molds for the bottom and upper layers were patterned in SU-8 photoresist (SU-8 2100, MicroChem Corp., Newton, MA, USA) via conventional photolithography. Post arrays for interconnecting holes were patterned in SU-8 on top of the bottom layer with precise alignment using an UV aligner (MA-4, Karl Suss, Garching, Germany). A thin PDMS (4:1 base to hardener mixture, Dow Corning, Midland, MI, USA) membrane was spin-coated on the master mold for bottom layer with post arrays. The spin speed (600 rpm for 30 s) was chosen to precisely control the membrane thickness to be slightly lower than the interconnect post height. The upper PDMS microchannel was prepared using conventional replica molding of PDMS (20:1 base to hardener mixture) from the SU-8 master for upper layer. The upper PDMS channel was aligned under a microscope and bonded on top of bottom PDMS membrane using oxygen plasma treatment (PDC-001, Harrick Plasma, Ithaca, NY, USA) and then peeled off along with the bottom layer. To assemble the final device, the multilayer PDMS channel was bonded with a slide glass *via* oxygen plasma and connected to tubing.

#### Preparation of PLGA-PEG NPs

PLGA<sub>10K</sub>-PEG<sub>5K</sub>, PLGA<sub>27K</sub>-PEG<sub>5K</sub>, PLGA<sub>45K</sub>-PEG<sub>5K</sub>, and PLGA<sub>95K</sub>-PEG<sub>5K</sub> (Boehringer Ingelheim GmbH, Ingelheim, Germany and Akina Inc., West Lafayette, IN, USA) was dissolved in acetonitrile (ACN, Sigma-Aldrich, St. Louis, MO, USA) at concentrations of 10-50 mg/mL. ACN and deionized water were employed as vertical and lateral sheath streams, respectively. While NPs can be prepared using different organic solvents, ACN was chosen because it is compatible with PDMS.<sup>29</sup> The PLGA-PEG precursor in ACN was introduced to the microchannel connected with the middle interconnecting holes. Pure ACN was introduced to the microchannel connected with the first and the third interconnecting holes. During the NPs synthesis, the flow rates were controlled by syringe pumps (Harvard Apparatus, Holliston, MA, USA) and the device was observed using an inverted microscope (Eclipse TS 100, Nikon, Tokyo, Japan). To confirm the vertical focusing, laser scanning confocal microspcope (LSM 510, Carl Zeiss Microscopy, Göttingen, Germany) was used. To obtain the confocal microscope images, aqueous solution of rhodamine 6G (Rh6G, Sigma-Aldrich, St. Louis, MO, USA) and fluorescein isothiocyanate (FITC, Sigma-Aldrich, St. Louis, MO, USA) were used as core and vertical sheath fluids, respectively. In case of the bulk synthesis,  $100 \,\mu\text{L}$  of polymeric precursor solution was mixed drop-wise with 1 mL of water for about 2 h under magnetic stirring. The resulting NP suspensions were purified by ultrafiltration using Amicon Ultracel 100 K membrane filters (EMD Millipore, Billerica, MA, USA), washed three times with water, and resuspended in water or PBS.

#### Characterization of PLGA-PEG NPs

The size distribution by volume fraction of PLGA-PEG NPs was measured using dynamic light scattering with Zetasizer Nano ZS (Malvern Instruments Ltd., Malvern, Worcs, UK). The synthesized PLGA-PEG NPs were imaged by TEM (200CX, JEOL, Tokyo, Japan) with negative staining by uranyl acetate (Electron Microscopy Sciences, Hatfield, PA, USA). For the release study, we dialyzed docetaxel-loaded NPs in 20 L of PBS, pH 7.4, at 37 °C using a 10 kDa cutoff membrane (Slide-A-Lyzer MINI Dialysis Devices, Thermo Scientific, Rockford, IL, USA). The amount of docetaxel released from the NPs was measured by HPLC (1100 Series, Agilent Technologies, Santa Clara, CA, USA).

#### In vivo pharmacokinetics (PK) and biodistribution

All experiments were conducted as approved by the MIT Committee on Animal Care (protocol #0710-055-13) and are in compliance with institutional and NIH guidelines. The procedures for the in vivo PK experiments were adapted from a method reported elsewhere.<sup>30–32</sup> For the *in vivo* experiments, 5 wt% Alexa-fluor 647 (Life Technologies, Grand Island, NY, USA) conjugated to PLGA45K (PLGA45K-A647) using 1-ethyl-3-(3dimethylaminopropyl)-carbo-diimide/N-hydroxysuccinimide chemistry was added to the polymeric precursor. Male and female Balb/c mice weighting 25 g were intravenously dosed with 5 mg of Alexa-fluor 647-labeled NPs via subclavian vein injection. At different time intervals (5, 15, 30 min, and 1, 2, 4, 6 h) 50  $\mu$ L of blood was sampled from the saphenous vein using a heparinized hematocrit capillary tube. To minimize the amount of blood removed on each animal, the different time-points were spread-out throughout the group to ascertain that each mouse was not sampled more than 5 times. Twelve hours after injection, a last blood sample was collected by cardiac puncture and the animals were euthanized by cardiac perfusion of PBS under deep anesthesia. Tissues (heart, lung, liver, spleen, and kidneys) were harvested for terminal biodistribution analysis (t = 12 h). Five animals were used in each group.

All samples were maintained on ice until analyzed for fluorescent quantification of NPs in plasma and organs (within 4 h). Blood samples were centrifuged at 2,000 rcf for 10 min, at 4 °C. The isolated plasma was collected and the volume was completed to 50  $\mu$ L with mouse plasma (Equitech-Bio, Kerrville, TX, USA). The fluorescence intensity was measured ( $\lambda_{ex}$ : 650 nm,  $\lambda_{em}$ : 665 nm) on a 96-well plate-reader (Tecan, Männedorf, Switzerland) and quantified using an 8-point calibration curve obtained from serial dilution in plasma of each formulation. The limit of quantification (LOQ) was determined as the lowest concentration for which the coefficient of variation in the calibration curve was below 10 % (19  $\mu$ g/mL). Samples with fluorescence below the LOQ were omitted. Moreover, to minimize the impact of fluorescence quenching in concentrated samples, samples with concentrations above 1,250  $\mu$ g/mL were further diluted until linearity in signal was achieved. The total concentration in plasma at each time-point was obtained by multiplying the concentration of each sample by the dilution factor used for preparation. The biodistribution data were obtained from imaging the organs on an IVIS molecular imaging system ( $\lambda_{ex}$ : 660 nm,  $\lambda_{em}$ : 680 nm). To account for the variability in the fluorescence of each formulation, the Total Radiant Efficiency was normalized by the slope of each calibration curve.

PK data were treated by non-compartmental analysis of plasma concentration *vs*. time profiles.  $C_{max}$  corresponds to the maximum concentration measured while  $C_0$  is extrapolated as the Y intercept of linear least-squares regression on the semilog plot of the plasma concentration *vs*. time curve.  $V_{d extrap}$  is determined by dividing the injected dose by  $C_0$ . The apparent first-order terminal elimination rate ( $K_{el}$ ) was estimated by linear least-squares regression on the semilog plot of the plasma concentration *vs*. time curve.  $t_{1/2}$  is equal to  $\ln^2/K_{el}$ . AUC<sub>0-t</sub> was calculated by the trapezoidal method from 0 to the last quantifiable timepoint. Areas under the blood concentration-time curve from time zero to infinity (AUC<sub>0-inf</sub>) were calculated by adding AUC<sub>0-12 h</sub> to the ratio of the last measurable concentration to  $K_{el}$ . Total Clearance was quantified as the injected dose divided by AUC<sub>0-inf</sub>.

Statistics were computed with SigmaPlot 11.0 software (Systat Software, Inc., San Jose, CA, USA). Differences in group means were calculated by standard unpaired *t* test or Mann–Whitney *U* test. The non-parametric tests were used if samples failed tests for equality of variance and/or normality with the Kolmogorov-Smirnov test. A value of P < 0.05 was considered significant. Table 1 lists which tests were used in each figure and table.

#### Results

#### Design and fabrication of multilayer PDMS microfluidic device

The fabrication process for the parallel 3D HFF device is illustrated in Figure 1. The parallel 3D HFF devices were obtained by casting PDMS on a master mold fabricated in SU-8 photoresist using two-step lithography. The spin speed was tuned to precisely control the PDMS thickness to be slightly lower than the interconnecting post height. The channel width at the vertical focusing region and mixing region were 100  $\mu$ m and 20  $\mu$ m, respectively. The height of upper and lower microchannels was fixed at 100  $\mu$ m.

Figure 2, *A* shows a photograph of the parallel 3D HFF device, with isolated upper (red) and lower (blue) layers filled with dye to highlight the geometries of the microchannels. Due to the two-layer design, the device is simplified and can be interfaced with only 3 inlets and 1 outlet tubing (Figure 2, *A*). 3D HFF was achieved by three sequential interconnecting holes for vertical focusing followed by a conventional cross junction for horizontal focusing.<sup>17</sup> The organic phases (i.e., polymer solution in ACN and pure ACN) were supplied from upper to lower layers through the three sequential interconnecting holes, visualized in Figure 2, *B* using red and green food coloring dyes to represent the PLGA-PEG polymer in ACN solution and pure ACN, respectively. The pure ACN streams focus the polymer stream vertically to isolate it from the top and bottom walls to prevent channel fouling, while the water stream focuses the organic streams horizontally to precipitate the NPs.<sup>17</sup> The device was designed with appropriate flow resistances to maintain an even distribution of flows to the parallel channels (Figure 2, *A* and *C*).

#### Simulation and experimental visualization of vertical focusing

The vertical focusing 3D HFF with three sequential inlets is strongly affected by the shapes of interconnecting holes. The effect of the geometry of the interconnecting holes on the vertical focusing was examined by using 3D finite element simulations using COMSOL (COMSOL Inc., Stockholm, Sweden) (Figure 3, A). Round interconnecting holes resulted in non-uniform distribution of concentration profiles. Likewise, rectangular interconnecting holes with lengths smaller than 100 µm resulted in arched vertical streams. The most uniform concentration profiles were achieved when rectangular interconnecting holes with lengths larger than 100 µm were used. Since larger SU-8 post arrays for replication of interconnecting holes may hinder the uniformity of thin PDMS layer during the spin coating process, the (streamwise) length of the interconnecting holes was fixed at 100  $\mu$ m. To verify the effect of the interconnect hole geometry, the performance of the multilayer 3D HFF device was examined using confocal microscopy with aqueous Rh6G (red) and FITC (green) fluorescent dye solutions as the polymer in ACN and ACN streams, respectively. As predicted by the simulations, more uniform vertical focusing could be achieved using rectangular interconnecting holes (100  $\mu$ m × 120  $\mu$ m) compared to circular holes (Figure 3, B and C).<sup>17</sup> The cross-section profiles and heights of the vertically focused streams obtained by confocal microscopy were also in good agreement with the 3D finite element simulations at various fractions of polymer flow in organic flow (f) (Figure 3, D and E).

#### Preparation and characterization of PLGA-PEG NPs

PLGA-PEG NPs with a range of sizes from 13 nm to 150 nm were prepared using the parallel 3D HFF device, demonstrating its utility for the synthesis of NPs with precise control over the particle size. To accomplish this size control, we varied both the PLGA block lengths (10, 27, 45, and 95 kDa) and polymer concentration in ACN (10–50 mg/mL) (Figure 4, *A*). For some conditions 2D HFF and the bulk synthesis method yielded polydisperse particles due to the aggregation of the polymeric precursor, whereas 3D HFF provided more homogeneous NPs. Figure 4, *B* shows the size distributions by volume

fraction of NPs synthesized from PLGA<sub>45K</sub>-PEG<sub>5K</sub> precursor at high concentrations (50 mg/ mL) using the three different methods (i.e., 3D HFF, 2D HFF, and bulk synthesis method). Here, the *f* of 3D HFF and 2D HFF were 0.7 and 1, respectively. Next, we; compared NPs prepared using the 8 parallel stream 3D HFF device to a single stream 3D HFF device fabricated in a similar manner. We observed that the size of NPs prepared with the single and 8 parallel 3D HFF was essentially identical within standard error (Figure 4, *C*). The size of NPs can be controlled simply by changing the flow ratio of polymer stream to the total flow rate of water (*R*).<sup>13,33</sup> When PLGA<sub>10K</sub>-PEG<sub>5K</sub> at high concentration (50 mg/mL) is used, the size drops from 26 nm to 13 nm as the *R* decreased from 0.2 to 0.02 (Figure 4, *D*). Similarly, NPs size decreased from 40 nm to 20 nm as the *R* decreased when PLGA<sub>27K</sub>-PEG<sub>5K</sub> at high concentration (50 mg/mL) is used (Figure 4, *E*). To further assess to potential of the platform for drug delivery purposes, we assembled drug-encapsulating NPs by bulk synthesis and parallel 3D HFF using PLGA<sub>10K</sub>-PEG<sub>5K</sub> as the polymeric precursor and docetaxel as a model therapeutic agent. In both cases, the NPs behaved similarly with 50 % of the drug release achieved after 5 h (Figure 4, *F*).

#### Proof-of-concept in vivo PK and biodistribution of small NPs

As a proof of concept, we utilized the microfluidic platform to study the biological behavior of NPs with two different sizes prepared by controlling the mixing time. *In vivo* PK and biodistribution were examined using Alexa-fluor 647 to label the NPs synthesized by the 8 parallel 3D HFF. Because Alexa-fluor 647 conjugated PLGA<sub>45K</sub> (PLGA<sub>45K</sub>-A647) was added to the PLGA<sub>10K</sub>-PEG<sub>5K</sub> precursor (5 wt%), the diameter of Alexa-fluor 647-labeled NPs was slightly increased compared to unlabelled NPs. At R = 0.04 and 0.2, the average diameters of Alexa-fluor 647-labeled NPs were 20 nm and 35 nm, respectively.

Interestingly, these NPs showed similar behavior when injected intravenously to mice without significant differences in circulation profiles and PK parameters (Figure 5, *A* and Table 1). Similarly, terminal distribution of the fluorescence in organs of the mononuclear phagocyte system (*i.e.*, liver, spleen, and lungs)<sup>32</sup> as well as the fluorescence in the kidneys and heart were comparable for both NPs (Figure 5, *B*).

#### Discussion

We demonstrated the parallelization of microchannels to increase production yield without impairing reproducibility, controllability, and robustness of microfluidic synthesis of NPs. In principle, the parallelization strategy could expand to clinically relevant production rates.<sup>9</sup> Recently, fabrication of parallelized PDMS microfluidic devices was demonstrated,<sup>23,24,26</sup> but manual drilling or punching that provide limited accuracy and repeatability between devices were used to fabricate the interconnecting holes. In 3D HFF with three sequential inlets, the lateral position of the inlet holes significantly affects the vertical focusing, which is difficult to control by manual drilling.<sup>17</sup> Instead, we defined the interconnecting holes in the parallel 3D HFF device by patterned SU-8 posts, which allowed for optimization of their cross-sectional geometry and excellent alignment with the microchannels. This approach reduced the manual interventions during the manufacturing process and resulted in lower variability of the chip-to-chip performance.<sup>34</sup>

The flow conditions of each 3D HFF unit in the 8 parallel 3D HFF device are designed to be the same as those in a single 3D HFF channel device. Therefore, the size of NPs prepared with the single and 8 parallel 3D HFF was essentially identical within standard error (Figure 4, *C*). In contrast, we observed a large difference between the 3D HFF and bulk synthesis (Figure 4, *C*). To achieve the same flow conditions in each 3D HFF unit in the 8 parallel 3D HFF device, the flow resistance in each channel should be precisely regulated. Since the flow resistance for laminar flow through a channel is proportional to the length of channel,

the microchannels were branched symmetrically to balance the flow resistances. In addition, the microchannel for the top sheath stream was meandered to balance the flow resistances (Figure 2, *C*). The upper and lower layers are separated by a PDMS membrane, but the pressure in the lower layer is much larger than that of upper layer. As a result, the PDMS membrane protrudes into the upper microchannels where the upper and lower microchannels cross, increasing the resistance of upper microchannel. The resistance increase is higher when the area of channel overlap region is larger. Since PDMS made of 4:1 base to hardener mixture is stiffer, 4:1 base to hardener mixture was used to minimize the protrusion of the PDMS membrane. In addition, the microchannels were branched off at the overlapping region to distribute the effect of resistance increase evenly. Since the parallel channels are coupled to each other, dust or aggregates of PLGA-PEG impede an even distribution of flow to the parallel channels. Square PDMS posts, which could filter out the dusts and aggregates, were therefore placed around the interconnecting holes (Figure 2, *B* and *C*).

Parallel 3D HFF devices were obtained by casting PDMS on a master mold fabricated in SU-8 photoresist using two-step lithography. Since the interconnecting holes between upper and lower PDMS channels were defined by patterned SU-8 posts, their shape could be optimized and excellent alignment of the holes and channels could be achieved. Because of the optimal shape and excellent alignment of interconnecting holes, the vertically focused stream did not touch the PDMS microchannels even at high f (f = 0.7). Therefore, NPs with uniform size distribution could be synthesized consistently in case of 3D HFF. However, 2D HFF and the bulk synthesis method yielded poly-disperse particles due to the aggregation of polymeric precursors in some cases.

Considering that the pure ACN sheath flows do not contain any NP precursors, this configuration allows us to maintain the yield of NPs while enabling robust operation of the system (Table 2). Minimal dilution of the precursor solution by pure ACN allowed the production rate of NPs to increase to 84 mg/h when 8 parallel 3D HFF was operated at high f(f = 0.7). This increase in yield shortens the preparation time for batches of NPs suitable for a series of *in vivo* mice experiments (25 mg) from over 5 h<sup>17</sup> to less than 20 minutes, which is critical to minimize drug release during NP synthesis. Furthermore, the NP production rate could be increased further by increasing the flow ratio as well as by increasing the number of parallel microchannels.

Many different organic solvents including tetrahydrofuran, acetone, and dimethylformamide have been used for conventional bulk NP preparation.<sup>5</sup> However, PDMS tends to swell in presence of many organic solvents, which would alter the fluid dynamics in the PDMS device. We used ACN and water for NP preparation because they are compatible with PDMS.<sup>29</sup> Other organic solvents including nitromethane, dimethyl sulfoxide, ethylene glycol, perfluorotributylamine, perfluorodecalin, and propylene carbonate can potentially be adopted for NP synthesis using our system as they do not swell PDMS.<sup>29</sup>

Since the size of NPs is one of the key factors that determine the biodistribution and therapeutic efficacy,<sup>3,8,32,35</sup> the ability to tune NPs size is important. We further established the potential of this platform by reproducibly synthesizing NPs with sizes tunable between 13 and 150 nm. Self-assembly of NPs under conditions of the most rapid mixing with lowest MW PLGA block (10 kDa) resulted in the smallest NPs (~13 nm diameter), which is very difficult to achieve with bulk synthesis methods. Similarly the highest MW PLGA block (95 kDa) and high polymer concentration resulted in the largest NP sizes (~150 nm diameter). Interestingly, all NPs had consistent average size batch-to-batch, and uniform size distribution.

In HFF devices, for fixed MW and concentration of polymeric precursor, the size of the NPs strongly depends on the mixing time ( $\tau_{mix}$ ), which can be estimated by equation (1).<sup>13,33</sup>

$$\tau_{mix} \sim \frac{w_f^2}{4D} \approx \frac{w^2}{9D} \frac{1}{\left(1 + 1/R\right)^2}$$
 (1)

Where *D* is diffusivity of the solvent,  $w_f$  is width of the focused stream, *w* is channel width, and *R* is the ratio of flow rate of the organic stream to the total flow rate of water. NPs obtained using the microfluidic channels are smaller than those synthesized from the bulk synthesis method because the  $\tau_{mix}$  is smaller than the characteristic aggregation time scale ( $\tau_{agg}$ ) (Figure 4, *D* and *E*).<sup>13</sup> In the current devices, Eq. (1) predicts  $\tau_{mix}$  in the range of 0.017–1.2 ms for typical flow ratios (R = 0.02-0.2). The influence of  $\tau_{mix}$  on the size of NPs disappears when  $\tau_{mix}$  is smaller than 0.066 ms (R = 0.04), suggesting that these NPs have reached the size limit for this specific copolymer.<sup>33</sup>

The ability to reproducibly synthesize small and monodisperse NPs exhibiting similar fate *in vivo* is particularly appealing in light of the recent literature reporting enhanced penetration of smaller NPs into solid tumors.<sup>36,37</sup> If NPs of two different sizes exhibit similar PK, we may expect the smaller NPs to be more effectively penetrate into solid tumors. Microfluidic platforms are advantageous for synthesis of small NPs by nanoprecipitation due to their ability to rapidly mix the precursors; NPs prepared by bulk nanoprecipitation tend to be larger.<sup>13,17,33</sup> A recent paper reported a different parallel flow focusing system that resulted in smaller NPs, although *in vivo* studies were not performed and the NP size was 50 - 200 nm.<sup>38</sup>

While is relatively simple to synthesize sub-30 nm inorganic NPs at large scales, it has remained challenging to synthesize polymeric NPs in this size range, especially loaded with drug and with controlled release properties. The parallel 3D HFF device enables the synthesis of small NPs with high production rates that allowed for *in vivo* studies. Since smaller NPs can penetrate more deeply into solid tumors,<sup>36,37</sup> parallel microfluidic synthesis has the potential to lead to the development of improved NPs with better drug delivery performance compared to larger NPs obtained by bulk synthesis. Therefore, the use of the parallel 3D HFF device to synthesize a variety of such NPs would likely prove a very valuable tool in the pre-clinical *in vivo* screening of these materials for cancer therapy.

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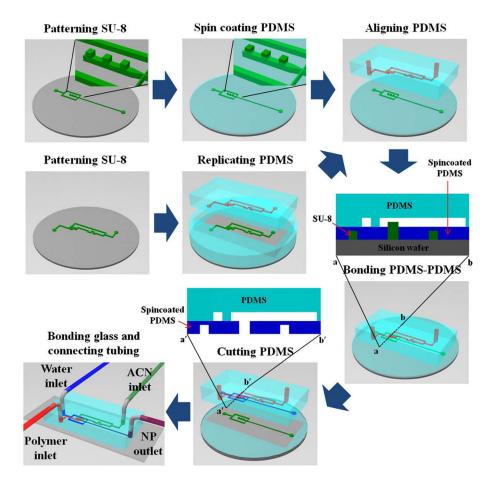
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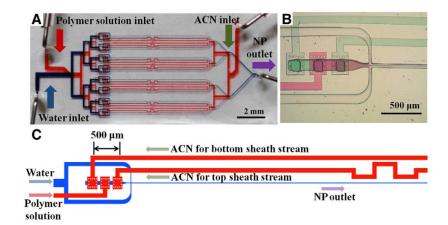
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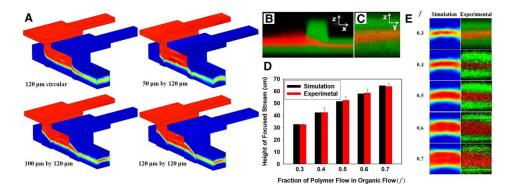
#### Figure 1.

3D Schematic illustration of fabrication procedure for the multilayer 3D HFF device. For clarity, the single channel 3D HFF device is depicted.



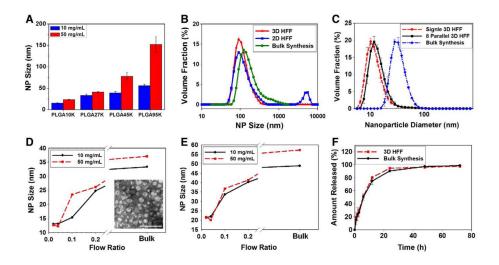
#### Figure 2.

3D HFF microfluidic device for parallel NP synthesis. (A) Device visualized using red and blue food coloring dyes in the upper and lower microchannels, respectively. PDMS was spin-coated thicker than the SU-8 post arrays (i.e., interconnecting holes were closed) to isolate the channels. (B) Optical microscope image of the 3D HFF region. Here, red and green food coloring dyes represent the PLGA-PEG polymer in ACN solution and pure ACN, respectively. (C) Schematic illustration of one of the 8 parallel 3D HFF units in the device.



#### Figure 3.

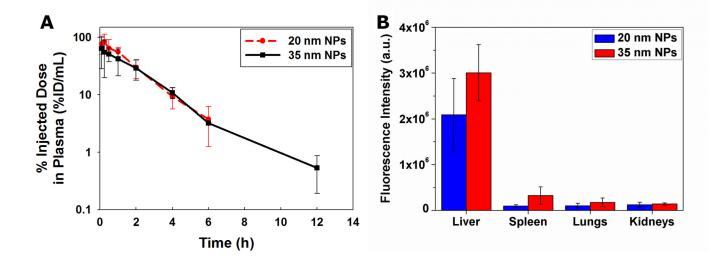
Vertical focusing in the 3D HFF device (Re = 0.833). Both width and height of the lower microchannel are 100  $\mu$ m. (**A**) Perspective views of 3D finite element simulations at the vertical focusing region with round (120  $\mu$ m in diameter), rectangular (50  $\mu$ m × 120  $\mu$ m), rectangular (100  $\mu$ m × 120  $\mu$ m), and square (120  $\mu$ m × 120  $\mu$ m) shapes of interconnecting holes. Here, the fraction of polymer flow in organic flow (*f*) is 0.3. (**B**) Cross-sectional side view and (**C**) cross-sectional front view of confocal microscopy images at the vertical focusing region when the fraction of polymer flow in organic flow (*f*) is 0.3. Width and length of interconnecting holes are 120  $\mu$ m and 100  $\mu$ m, respectively. Fluid flows in the *x*-direction after focusing. (**D**) Height of vertically focused polymeric stream as a function of *f*. (**E**) Cross-sectional side view from the 3D finite element simulation and confocal microscope images at the vertical focusing region as a function of *f*.



#### Figure 4.

NP synthesis and drug release. (A) Effect of PLGA-PEG precursor concentrations on the size of synthesized PLGA-PEG NPs depending on the MW of polymeric precursors (f = 0.7, R = 0.1). (B) The size distribution by volume fraction of NPs prepared from PLGA<sub>45K</sub>-PEG<sub>5K</sub> by microfluidic 3D HFF at (f = 0.7, R = 0.1), 2D HFF (f = 1, R = 0.1), and bulk synthesis method. Here, the precursor concentration was 50 mg/mL. (C) The size distribution by volume fraction of NPs prepared from 10 mg/mL PLGA<sub>10K</sub>-PEG<sub>5K</sub> by single 3D HFF, 8 parallel 3D HFF, and bulk synthesis (f = 0.7, R = 0.04). (D, E) Effect of flow ratio on NPs size prepared from (D) PLGA<sub>10K</sub>-PEG<sub>5K</sub> and (E) PLGA<sub>27K</sub>-PEG<sub>5K</sub> by 3D HFF at f = 0.7. NPs prepared by 3D HFF were smaller in size than those obtained by bulk synthesis. The inset shows TEM image of the NPs prepared by 3D HFF (f = 0.7, R = 0.04). Scale bar is 100 nm. (F) Docetaxel release profile of NPs prepared from 50 mg/mL PLGA<sub>10K</sub>-PEG<sub>5K</sub> by 3D HFF and bulk synthesis.

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#### Figure 5.

PK and biodistribution in mice of small NPs synthesized by 3D HFF. (**A**) The systemic circulation lifetime of Alexa-fluor 647-labeled PLGA<sub>10K</sub>-PEG<sub>5K</sub> NPs prepared with two different flow ratios to tune the size (R = 0.04 and 0.2 for 20 nm and 35 nm diameters, respectively). (**B**) The fluorescence intensity per organ of Alexa-fluor 647-labeled NPs at 12 h from intravenous injection. Five animals were used in each group. Both NPs showed similar behavior when injected intravenously to mice without significant differences in circulation profiles, PK parameters, and terminal distribution of the fluorescence in organs.

#### Table 1

The summary of calculated PK parameters, *P* values, and statistical test methods.

	20 nm NPs	35 nm NPs	P value	Statistical test
Half-life (h)	$1.3\pm0.19$	$1.7\pm0.30$	p = 0.095	Mann-Whitney
Ke (h <sup>-1</sup> )	$0.5\pm0.09$	$0.4\pm0.09$	p = 0.095	Mann-Whitney
AUC <sub>0-12h</sub> (%ID.h.mL <sup>-1</sup> )	$168\pm56$	$156\pm61$	p = 0.371	t-test
AUC <sub>0-inf</sub> (%ID.h.mL <sup>-1</sup> )	$169\pm56$	$157\pm62$	p = 0.378	t-test
V <sub>d extrap</sub> (mL)	$1.2\pm0.50$	$2.0\pm0.83$	p = 0.055	t-test
V <sub>d area</sub> (mL)	$1.3\pm0.84$	$1.8\pm0.74$	p = 0.186	t-test
Clearance (mL/h)	$0.7\pm0.37$	$0.7\pm0.23$	p = 0.461	t-test
C <sub>max</sub> (%ID.mL <sup>-1</sup> )	$81\pm25$	$72\pm27$	p = 0.301	t-test

#### Table 2

The production rate of NPs and time required for synthesis of 25 mg of NPs for single flow focusing and 8 parallel flow focusing, respectively. Here, the flow ratio were fixed at R = 0.1.

	Single 3D HFF $(f = 0.3)^{17}$	Single 3D HFF ( $f = 0.7$ )	8 3D HFF ( $f = 0.7$ )
Flow rate of polymeric precursor	1.5 μL/min	3.5 µL/min	28 μL/min
Flow rate of water	$50 \mu\text{L/min}$	$50\mu\text{L/min}$	$400\mu\text{L/min}$
Polymer concentration	50 mg/mL	50 mg/mL	50 mg/mL
Production rate	4.5 mg/h	10.5 mg/h	84 mg/h
Time for 25 mg NPs	334 min	143 min	18 min