Notes on Resilience Measures

Citation

Permanent link
https://nrs.harvard.edu/URN-3:HUL.INSTREPOS:37374719

Terms of Use
This article was downloaded from Harvard University’s DASH repository, and is made available under the terms and conditions applicable to Other Posted Material, as set forth at http://nrs.harvard.edu/urn-3:HUL.InstRepos:dash.current.terms-of-use#LAA

Share Your Story
The Harvard community has made this article openly available. Please share how this access benefits you. Submit a story.

Accessibility
NOTES ON RESILIENCE MEASURES

William C. Clark

July 1975

Working Papers are not intended for distribution outside of IIASA, and are solely for discussion and information purposes. The views expressed are those of the author, and do not necessarily reflect those of IIASA.
MEMORANDUM

To: CS Holling
From: Bill Clark
Date: 22 July 1975
Subject: Notes on Holling's Resilience Measures Presentation (IIASA, 11 July 1975)

The following points are taken from my notes on the resilience measures. I don't necessarily agree with or understand all of them, but they should probably be dealt with explicitly before a final document is prepared.

A. SIMPLE MODELS FOR RESILIENCE MEASURES

You make the point that we are developing the present approach as "the simplest possible case," for largely pedagogic and learning purposes. But the prey-predator (PP), 2-dimensional state space representation is not the simplest case; the single dimension (say, "prey") case is. Almost every point made in the presentation could have been done more clearly on a one dimensional axis:

```
  ________________
 /                     /
|                     |
|  equilibrium B      |
|                      |
|  domain (B)         |
|____________________|
                  x
              domain (A) of stability, with two boundary points
```

This one-dimensional case is not trivial and serves to highlight many of the ideas which concern us.

Many of the empirical cases (especially design ones) to which we wish to apply R measures are essentially single dimensioned (see my WP examples, especially Tocs Island) and we force them into wondrous contortions when we attempt to make PP cases for their state spaces. My guess is that most actual cases will be more realistically interpreted and clearly understood as one dimensional R problems.

cc:
Messrs: Jones, Rashid, Bell, Häfele, Gruemm, Walters, Hilborn, Steele, Casti, Swain, Rinaldi
B. PERTURBATIONS AND RESILIENCE

Steele suggested that $R$ is defined usefully only by the system and the perturbation. He guessed that the really difficult thing was going to be specifying the nature of the perturbations in a meaningful way. Several related notions emerge:

1) **Perturbation Structure**: Since in most biological systems $X \propto X^2$, the perturbation structure $\Delta X \propto aX$ with (a) a positive constant might be most realistic. But $\Delta X \propto 1/bX$ with (b) a positive constant might be more dangerous because of control pathologies, etc. (Perturbations get proportionally greater as $X$ gets closer to zero.)

2) Holling's approach takes the relevance of the perturbation into his $R$ measures via his log-transform arguments; Hafele does not.

3) **Relation to components and hazard typology work**: Steele's point that $R$ is a function of both system and perturbation is of course an idea we have encountered previously. We (and the Energy Group) rejected it largely in the hope of developing a $R$ concept explicitly free of assumptions about the (unknown, surprising) perturbations which would occur.

   Note however that in my empirical components work I almost always end up trying to characterize the character of the perturbation in addition to - or even instead of - that of the system. This approach is carried to its extreme in the Kate-White-Slovic
Typology of Hazards notions. Furthermore, my components theory note of January 1975 discusses Class I phenomena in a context explicitly defined by the scale of the relevant perturbation.

Altogether it seems that we might do well to reconsider explicit integration of perturbation structure into the R concept and R-measures. This has a certain attractiveness to it in that it lets you begin shifting your concern from the detailed nature of the system (which by premise is unknown) to the general character of the perturbations. And if the Kates-White-Slovic typology arguments stand up under examination, and can be cast somewhat more generally, then "the general character of perturbations" may be something which we can in fact get a handle on.

Points to pursue in this context would include viewing the components as structures which could be applied to particular hazard types, and trying to cast R measures as a function of perturbation and components alone, with little or no reliance on detailed character of the system (the latter being again, by premise, unknown).
C. DIMENSIONAL ANALYSIS AND R-MEASURES

Steele also raised the possibility of using dimensionality arguments in designing R-measures. This has been touched on in your note of the 15 July working session, but the following notions might also be noted:

We have been criticized by many for the dependence of some of the proposed R-measures on the scales of the state-space. For generality, we must strive for dimensionless measures. In practice, this may consist of nothing more than the approach implied in my January 1975 Resilience note: i.e. defining "the system" with respect to the perturbation.

In general, both state space behavior and perturbation effect can be expressed as some combination of "length" (L) and "time" (T). The dimensions should almost certainly be included in any R-measure (Instantaneous perturbations and point locations can be dealt with as special cases "in the limit").

The following table began to emerge during the discussions. I would hope it could be recast and completed perhaps including your 15 July table (attached).
### Assumptions

<table>
<thead>
<tr>
<th>Assumption</th>
<th>Most Specific R-Measure Available</th>
<th>Dimensions</th>
</tr>
</thead>
<tbody>
<tr>
<td>1) No expectation of location in state space</td>
<td>area of stable basin</td>
<td>$L^n$</td>
</tr>
<tr>
<td>2) Probability expectation of location over some time period</td>
<td>expected distance to edge over same period</td>
<td>$E(L)/T$</td>
</tr>
<tr>
<td>3) Given trajectory over same period</td>
<td>average distance to edge over same period</td>
<td>$L/T$</td>
</tr>
<tr>
<td>4) Given location at a specific time (time in the limit?)</td>
<td>distance to edge</td>
<td>$L/\text{?}T$</td>
</tr>
</tbody>
</table>

I think the dimensions may be wrong here, and maybe we should follow earlier comments in revising it explicitly incorporating a column on "type of perturbation" giving the latter dimensions as well.

Finally it was suggested, and I shall record without understanding, that any time a R-measure was cast as a dimensionless number (say, as a perturbation in $LT^{-1}$ over a trajectory in $LT^{-1}$), we were left with a probability (a dimensionless number). This feels quite wrong, but surely we have often viewed R-measures precisely in the "probability-of-persistence" context, (see my January 1975 note, and Neil Gilbert's critique of my 1974 NRC-Status Report write-up). The question remains as to how, the probability-of-persistence and dimensionless-number R-measures are related.
D) R-MEASURE "CLASSES" (in a system, of a system, for a system..)

As you know, I feel that we have been unjustifiably sloppy in our use of terminology here. While I concur with your "Good Afternoon Wolf" reply to Casti's jargon criticism, the conventions adopted in the 15 July "Summary" table are bound to lead to great confusion. One difficulty hangs on the uncritical use of the word "system". Which system? That defined by the perturbation? That including Restorative Components? That encompassing Contingency Component elements? I don't insist that we address these other aspects of Resilience in a measurement sense now, but we should make use of what we know about them in our choice of terms.
<table>
<thead>
<tr>
<th>CLASS</th>
<th>PERTURBATION</th>
<th>TRANSFORM</th>
<th>EQUATION</th>
<th>DIMENSIONS</th>
<th>REMARKS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Resilience within a system</td>
<td>State Variable</td>
<td>any</td>
<td>Multiplicative $(I = cx)$</td>
<td>log.</td>
<td>$R = \frac{\int_A \rho(x,y) \varphi(x,y) , dx , dy}{\int_A \varphi(x,y) , dx , dy}$</td>
</tr>
<tr>
<td>Resilience of a system</td>
<td>Parameter</td>
<td>-&quot;-</td>
<td>-&quot;-</td>
<td>log.</td>
<td>$R = \frac{1}{\int_s \frac{ds}{dt} \rho(s)}$</td>
</tr>
<tr>
<td>Trajectory Resilience</td>
<td>Dist. Variable</td>
<td>-&quot;-</td>
<td>Constant $(I = c)$</td>
<td>none</td>
<td>$R = \frac{1}{\int_t^t \frac{dt}{\rho(t)}}$</td>
</tr>
<tr>
<td>Time fixed</td>
<td>State Variable</td>
<td>-&quot;-</td>
<td>Multiplicative $(I = cx)$</td>
<td>log.</td>
<td>$R = \frac{1}{\int_0^t \rho(t) , dt}$</td>
</tr>
</tbody>
</table>

NOTE 1: We have left out a class which is essential, i.e., policy resilience

SUMMARY OF RESILIENCE DISCUSSIONS, 15 JULY 1975