Excitable Patterns in Active Nematics

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(Dated: November 18, 2010)

We analyze a model of mutually-propelled filaments suspended in a two-dimensional solvent. The system undergoes a mean-field isotropic-nematic transition for large enough filament concentrations and the nematic order parameter is allowed to vary in space and time. We show that the interplay between non-uniform nematic order, activity and flow results in spatially modulated relaxation oscillations, similar to those seen in excitable media. In this regime the dynamics consists of nearly stationary periods separated by “bursts” of activity in which the system is elastically distorted and solvent is pumped throughout. At even higher activity the dynamics becomes chaotic.

Colonies of motile microorganisms, the cytoskeleton and its components, cells and tissues have much in common with soft condensed matter systems (i.e. liquid crystals, amphiphiles, colloids etc.), but also exhibit phenomena that do not appear in inanimate matter. These unique properties arise when the constituent particles are active: they consume and dissipate energy to fuel internal changes that generally lead to motion. When active particles have elongated shapes, as seen in cytoskeletal filaments and some cells, they undergo orientational ordering at high concentration to form liquid crystalline phases. The theoretical and experimental study of active materials has disclosed a wealth of emergent behaviors realizable in active materials and the connection between material characteristics and system dynamics remain incompletely understood. In this letter, we show that active systems exhibit behaviors similar to those of excitable systems, showing relaxation oscillations that couple activity to spontaneous pulsatile flow with quiescent periods in between, similar to biological pumps. We furthermore show that systems which undergo nematic ordering can give rise to large-scale swirling motions resembling those observed in Ref. [5] even in the absence of polar order. These behaviors were not seen in previous investigations because they arise only when the degree of nematic order is allowed to fluctuate in space and time.

Our model consists of mutually-propelled elongated particles suspended in a solvent confined to two dimensions, as seen for example in recent motor-filament assays [5]. The dynamical variables in such a system are particle concentrations $c$, the solvent flow field $v$ and the nematic tensor $Q_{ij}$, with $S$ the nematic order parameter and $n$ the director field, all of which are allowed to vary in space and time. We assume that the suspension of rod-like active particles have length $\ell$ and mass $M$ in a solvent of density $\rho_{\text{solvent}}$. The total density of the system $\rho = Mc + \rho_{\text{solvent}}$ is conserved, so the fluid is assumed to be incompressible. The total number of active particles is also constant, thus the concentration $c$ obeys the continuity equation:

$$\partial_t c = -\nabla \cdot (j^p + j^a),$$

where $j^p$ and $j^a$ are respectively the passive and active contributions to the current density. The passive current density has the standard form $j_i^p = cv_i - D_i\delta_j c$ where $D_{ij} = D_0\delta_{ij} + D_1Q_{ij}$ is the anisotropic diffusion tensor, while the active current can be constructed phenomenologically to be of the form $j_i^a = -\alpha c^2\partial_j Q_{ij}$ or derived from microscopic models [6]. Here the factor $c^2$ reflects the fact that activity arises from interactions between pairs of rods while the constant $\alpha$ describes the level of activity and is proportional to the concentration of motors and the rate of adenosine-triphosphate (ATP) consumption.

The flow velocity obeys an active form of the Navier-Stokes equation

$$\rho \partial_t v_i = \eta \Delta v_i - \partial_i p + \partial_j \tau_{ij},$$

with $\eta$ the viscosity, $p$ the pressure, and the active stress tensor $\tau_{ij}$ given by:

$$\tau_{ij} = -\lambda S H_{ij} + Q_{ik}H_{kj} - H_{ik}Q_{kj} + \alpha c^2 Q_{ij}$$

(3)

Here $\nabla \cdot v = 0$, and the first three terms in Eq. (3) represent the elastic stress due to the liquid crystalline nature of the system, with $H_{ij} = -\delta F/\delta Q_{ij}$ the molecular tensor defined from the two-dimensional Landau-De Gennes free energy:

$$F/K = \int dA \left[ \frac{1}{2} (\nabla \cdot Q)^2 + \frac{1}{4}(c^* - c) \text{tr} Q^2 + \frac{1}{2}c(\text{tr} Q^2)^2 \right]$$

where $K$ is the splay and bending stiffness in the one constant approximation. At equilibrium, above the crit-
and the molecular tensor $H_u$.

Constructing all possible traceless-symmetric combinations produced in Ref. [8] and represents the tensile/contractile nematic (IN) transition is driven only by the concentration $c$ of the nematogens. The last term was first introduced in Ref. [9] and represents the tensile/contractile stress exerted by the active particles in the direction of the director field $n$ with $\alpha_2$ a second activity constant.

Finally, the nematic order parameter $Q_{ij}$ satisfies a hydrodynamic equation that can be obtained by constructing all possible traceless-symmetric combinations of the relevant fields, namely the strain-rate tensor $\nu_{ij} = \frac{1}{2}(\partial_i v_j + \partial_j v_i)$, the vorticity tensor $\omega_{ij} = \frac{1}{2}(\partial_i v_j - \partial_j v_i)$ and the molecular tensor $H_{ij}$ [7], so that

$$[\partial_t + v \cdot \nabla] Q_{ij} = \gamma^{-1} H_{ij} + \lambda S u_{ij} + Q_{ik} \omega_{kj} - \omega_{ik} Q_{kj}$$

(4)

where $\gamma$ is an orientational viscosity, and the additional terms on the right-hand side describe the coupling between nematic order and flow in two dimensions, with $\lambda$ the flow-alignment parameter which dictates how the director field rotates in a shear flow and affects the flow and rheology of active systems [2, 3].

The dynamics of such an active nematic suspension is governed by the interplay between the active forcing, whose rate $\tau_a^{-1}$ is proportional to the activity parameters $\alpha_1$ and $\alpha_2$, and the relaxation of the passive structures, the solvent and the nematic phase, in which energy is dissipated or stored. The response of the passive structures, as described here, occurs at three different time scales: the relaxation time scale of the nematic degrees of freedom $\ell^2/(\gamma^{-1} K)$, the diffusive time scale $\ell^2/D_0$, the dissipation time scale of the solvent $pL^2/\eta$, where $L$ is the system size. While the presence of three dimensionless parameters makes for a very rich phenomenology, we typically assume that the three passive time scales are of the same magnitude $\tau_p$. When $\tau_a \gg \tau_p$, the active forcing is irrelevant and the system is just a traditional passive suspension. On the other hand, when $\tau_a \sim \tau_p$, the passive structures can balance the active forcing leading to a stationary regime in which active stresses are accommodated via both elastic distortion and flow. Finally, when $\tau_c \ll \tau_p$, the passive structures will fail to keep up, leading to a dynamical and possibly chaotic interplay between activity, nematic order and flow. In the rest of the paper, we quantify these different regimes. We first make the system dimensionless by scaling all lengths using the rod length $\ell$, scaling time with the relaxation time of the director field $\tau_p = \ell^2/(\gamma^{-1} K)$ and scaling stress using the elastic stress $\sigma = K \ell^{-2}$.

We start with a linear stability analysis of the hydrodynamic equations about the homogeneous solution letting $\varphi = \{c, Q_{xx}, Q_{xy}, 2 \omega_{xy}\} = \varphi_0 + \delta \varphi(t)$ with $\varphi_0 = \{c_0, S_0/2, 0, 0\}$, and consider solutions with periodic boundary conditions on a square domain of the form

$$\delta \varphi(x, t) = \sum_{n=-\infty}^{\infty} \sum_{m=-\infty}^{\infty} \varphi_{nm}(t) \exp\left[\frac{2\pi i}{L}(nx + my)\right]$$

With this choice the linearized hydrodynamic equations reduce to a set of coupled linear ordinary differential equations for the Fourier modes $\varphi_{nm}$: $\partial_t \varphi_{nm} = A_{nm} \varphi_{nm}$. The first mode to become unstable is the transverse excitation $(n, m) = (0, 1)$ associated with the block-diagonal matrix:

$$A_{01} = \begin{pmatrix} a_{01} & 0 \\ 0 & b_{01} \end{pmatrix}$$

where:

$$a_{01} = \left( -\frac{\pi^2}{L^2} (2D_0 - D_1 S_0) \frac{4\pi^2}{L^2} \alpha_1 c_0 - \frac{4\pi^2}{L^2} \right)$$

and:

$$b_{01} = \left( \frac{4\pi^2}{L^2} \alpha_2 c_0 - \frac{4\pi^2}{L^2} S_0 (1 - \lambda) \frac{1}{2} (1 - \lambda) S_0 \right)$$

(5)

The mechanism that triggers the instability of the homogeneous state relies on the coupling between local orientations and flow embodied in the matrix $b_{01}$, whose diagonalization yields a lower critical value of $\alpha_2$:

$$\alpha_2^* = \frac{4\pi^2 [2\eta + S_0^2 (1 - \lambda)^2]}{c_0 L^2 S_0 (1 - \lambda)}.$$
FIG. 2: (Color online) The hydrodynamic fields $c$, $S$, $\theta$ and $v_x$ along the $y$ axis for $\alpha_2 = 0.4$. The yellow region indicates the band visible in the top panels of Fig. 1.

with the viscosity of the solvent. In general, shear flow causes the director field to rotate for $\lambda \neq 1$, which generates elastic stress. For small activity, the elastic stiffness dominates and suppresses flow, while above $\alpha_2^*$ we observe collective motion.

To go beyond this simple analysis, we numerically integrated the hydrodynamic equations on a two-dimensional periodic domain with initial configurations of a homogeneous system whose director field was aligned along the $x$ axis subject to a small random perturbation in density and orientation, with $\alpha_1 = \alpha_2/2$, $\eta = c^* = D_0 = D_1 = 1$, $\lambda = 0.1$ and $L = 10$. As predicted by the linear stability analysis, at low activity the system relaxes to a stationary homogeneous state with $v_x = v_y = 0$ and $S = \sqrt{1 - c^*/c}$. Above the critical value $\alpha_2^*$, the system forms two bands flowing in opposite directions. The solution is constant along the flow direction (see Fig. 1) while the direction of the streamlines (in this case along the $x$ direction) is dictated by the initial conditions. As shown in Fig. 2, the optimta in the flow velocity correspond to the maximal distortion of the director field $n$. Variations in concentration $c$ and the nematic order parameter $S$ are of order 2% with a minimum in $S$ at the center of a flowing band due to the balance between diffusive and active currents. We note that these density modulations parallel to the nematic director are characteristic of systems with nematic order, while the density bands orthogonal to the direction of alignment observed in Ref. [5] are consistent with polar order [2].

Upon increasing the value of the activity parameter $\alpha_2$, the spontaneously flowing state evolves into a pulsatile spatial relaxation oscillator. Fig. 3 (top left panel) shows a plot of the $x$ and $y$ component of the flow velocity in the center of the box for $\alpha_2 = 1.5$. In this regime the dynamics consists of a sequence of almost stationary passive periods separated by active “bursts” in which the director switches abruptly between two orientations. During passive periods, $c$ and $S$ are nearly uniform, there is virtually no flow and the director field is either parallel or perpendicular to the $x$ direction. Eventually this configuration breaks down and the director field rotates by $90^\circ$ (see Fig. 3). The rotation of the director field is initially localized along lines, generating a band of flow similar to those in Fig. 1 (top). The flow terminates after the director field rotates and a uniform orientation is restored. The process then repeats.

This rotation of the director field occurs through a temporary “melting” of the nematic phase. As shown in Fig. 3, during each passive period the nematic order parameter is equal to its equilibrium value $S_0 = \sqrt{1 - c^*/c}$, but drops to $\sim 2/5 S_0$ during rotation. The reduction of order is system-wide, but, as shown in the middle in the bottom-left panel of Fig. 3, is most pronounced along the boundaries between bands. Without transient melting, the distortions of the director field required for a burst are unfavorable for any level of activity.

To illustrate the origin of the relaxation oscillations it is useful to construct a simplified version of the hydrodynamic equations by retaining the minimal features responsible for the oscillatory phenomenon: the coupling between active forcing and the fluid microstructure and
with positions related to “grains” in which the director spectively. The flow is characterized by large vortices (bottom) shows a typical snapshot of the flow velocity not occur in our equations unless the magnitude of the tory dynamics and the chaotic flows discussed below do and eventually chaotic. We emphasize that the oscilla-

of low activity periods and bursts becomes more complex

and

where $\alpha < \frac{1}{4}(2a + k^2)$ the system rapidly relaxes to a state characterized by a finite strain-rate that bal-

where $k$ is a wave number of an arbitrary spatial mode and $a$ and $b$ are constants. Eqs. (6) has the form of the FitzHugh-Nagumo model for excitable dynamical sys-
mics. For $\alpha < \frac{1}{4}(2a + k^2)$ the system rapidly relaxes to a state characterized by a finite strain-rate that bal-

As anticipated, when the active and passive time-scales are comparable the active forcing is accom-
mic system. Thus the dynamics in this

field is uniformly oriented. The grain boundaries are of the order of the system size and are the fastest flow-

In summary, we analyzed the hydrodynamics of active nematic suspensions in two dimensions. By allowing spatial and temporal fluctuations in the nematic order parameter we have observed a rich interplay between or-

We gratefully acknowledge support from the NSF Brandeis MRSEC (LG, BC, and MFH), the NSF Harvard MRSEC (LG,LM), NIAID R01AI080791 (MFH), the Harvard Kavli Institute for Nanobio Science & Technology (LG, LM), and the MacArthur Foundation (LM).
